

Ares 1X Hybrid Modeling with Comparisons to Flight Data



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Integrated Loads, Structures, and Mechanisms 10 June 2010







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### Outline



- Ares 1X Flight Summary
- Ares 1X Data Summary
- Model Descriptions
- Model Comparisons to Flight Data
  - Liftoff
  - Transonic
  - RCS Firings
- Observations and Lessons Learned



### Ares 1X Test Flight October 28<sup>th</sup>, 2009





- Flight objectives included characterization of acoustic and random vibration environments
- Assessment of the vibroacoustic modeling methods possible



## Significant Flight Events

Possible Environment Drivers

### Transonic





### **Roll Control Firings**



- Peak Liftoff Pressures occurred at T = 3-5 sec
- Transonic occurred at T = 22-39 sec
- Roll Control Firings occurred 11 times throughout flight



### Ares 1X Flight Data Summary



- Low Frequency Channels (up to 100-150 Hz)
  - Under review: 42 accelerations and 243 pressures
- High Frequency Pressures (up to 1250 or 2500 Hz)
  - 5 of 60 channels did not produce good data
- High Frequency Accelerations (up to 1250 or 2500 Hz)
  3 of 21 channels did not produce good data
- Data Validity and Filtering for HF Channels
  - An anti-aliasing filter was applied to the raw data at 4x the sample rate
  - Data for the ~5200 samples/sec channels are good to about 1000-1250 Hz
  - Data for the ~10400 samples/sec channels are good to about 2500 Hz



## SEA and Hybrid Models

Multi-model approach

- SEA Models built from FEM as a preflight exercise
- External Pressure Loading
  - Representative flight pressures applied
- Standard Damping
  - 1% loss factor
- Standard Cavity Absorption
  - 1% absorption
- SIF Applied to All External Surfaces
- Hybrid models built with local detail then integrated into full-stack SEA models
- Hybrid Connections
  - Manual hybrid line connections used at FE/SEA I/F







## Liftoff Reconstruction Analysis

Flight time 4 to 4.5 seconds



- SEA and SEA/FE hybrid model results compared to processed flight data (20-1000 Hz for 5200 sample rate, 20-2000Hz for 10400 sample rate)
- Processed flight data for pressures and accelerations at the 4 4.5 second interval
- Applied flight pressures to the model and recovered accelerations at the locations corresponding to the flight instrumentation
- No adjustments to the models or modeling parameters were made post flight

Pressure Time History





## Liftoff PSDs (T = 4-4.5s)

Forward Vehicle Section







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Model vs. Flight Data



#### SEA greatly over predicts at frequencies of low modal density, whereas the hybrid model is very accurate by accounting for the discrete modes



Honoring the Legect:

Issuring the

Model vs. Flight Data



#### Lack of FE model fidelity is most likely the cause of the poor correlation <50Hz

OEING



Model vs. Flight Data



#### Poor correlation most likely from the inability to capture correct CM Panel response

DEING

## Transonic Reconstruction Analysis

Flight time 35.5 to 36.0 seconds

- Y E A R S Assuring the Mission.
- SEA and SEA/FE hybrid model results compared to processed flight data (20-1000 Hz for 5200 sample rate, 20-2000Hz for 10400 sample rate)
- Due to the widely varying pressures and minimum and maximum pressure level were used
- Applied TBL loading for M=0.85 with default parameters
  - Distance from leading edge modified to the distance from the vehicle nose







### Transonic PSDs (T = 35.5-36.0s)

Forward Vehicle Section



DEING



## Transonic Response Comparison

Model vs. Flight Data



## High frequency over prediction occurs just above the ring frequency of the panel

DEING

14



## Transonic Response Comparison

Model vs. Flight Data



![](_page_14_Picture_3.jpeg)

![](_page_14_Picture_4.jpeg)

## Instrument location is a significant factor in assessing the accuracy of the model predictions

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## **Roll Control Thruster Firings**

Flight time 8.5 seconds

![](_page_15_Picture_2.jpeg)

![](_page_15_Figure_3.jpeg)

![](_page_15_Figure_4.jpeg)

![](_page_15_Picture_5.jpeg)

- Thruster firings induced significant vibrations in the first and upper stages
- Data and modeling assessment completed to determine the source of the vibration and the ability to simulate the event

![](_page_15_Picture_8.jpeg)

### Acoustic or Mechanical Driven?

Data Assessment

![](_page_16_Picture_2.jpeg)

 The trend of the pressure increase equal to or greater than the increase in acceleration response, implies that most of the response is <u>thruster plume acoustic driven</u>

![](_page_16_Figure_4.jpeg)

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## **RCS Firing SEA/Hybrid Modeling**

Multi-model approach

- Model First Stage Avionics Module (FSAM) location during a time while RCS is firing and a time without
- Apply the time consistent pressures and compare the change in predicted response to the flight response
- Partially integrated model broken into 4 loading zones

![](_page_17_Figure_5.jpeg)

Moring the Legal

**Zone** A

**Zone B** 

Zone C

## Nominal Flight Response Comparison

Model vs. Flight Data

![](_page_18_Figure_2.jpeg)

#### characteristics of the FSAM

## **RCS Firing Response Comparison**

Model vs. Flight Data

![](_page_19_Figure_2.jpeg)

Given that the simulation is linear, the increase in pressure captures the correct response...the firings can be modeled!

TEING-

Time [sec]

### **Observations and Lesson Learned**

![](_page_20_Picture_1.jpeg)

- Multi-model hybrid method
  - Quick model set-up with an attractive computational cost when compared to full vehicle FEM or BEM
  - Hybrid results matched well with full vehicle FEM on another program
  - SEA not valid in the bulk of the frequency range of interest in many cases
- Building Experience
  - Model fidelity was a key player in the degree of correlation to test data
  - Instrumentation location during flight or in tests critical for model correlation
  - Correlating models for vibrations due to <u>aero-acoustics</u> may require a more controlled environment than the flight test
  - <u>RoCS events are significant</u> for random vibration and they can be predicted though modeling

This flight has provided tremendous knowledge on modeling launch vehicle vibroacoustics and much more like it need to occur

![](_page_20_Picture_12.jpeg)

![](_page_21_Picture_0.jpeg)

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![](_page_21_Picture_2.jpeg)

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![](_page_21_Picture_6.jpeg)

![](_page_21_Picture_7.jpeg)

![](_page_21_Picture_8.jpeg)

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![](_page_22_Picture_0.jpeg)

# Thank you

![](_page_22_Picture_2.jpeg)

![](_page_22_Picture_3.jpeg)

![](_page_22_Picture_4.jpeg)

![](_page_22_Picture_5.jpeg)

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Model vs. Flight Data

![](_page_23_Figure_2.jpeg)

## The SM area is modeled as a simple panel and it is evident from the CAD picture that there is much more structure required for an accurate prediction

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![](_page_23_Picture_7.jpeg)

Model vs. Flight Data

![](_page_24_Figure_2.jpeg)

#### The instrument is mounted directly next to flight avionics but SEA bare panel response slightly under predicts, most likely due to model fidelity

![](_page_24_Picture_5.jpeg)

![](_page_24_Picture_8.jpeg)

Location