

# DERIVATION OF MILES EQUATION FOR THE RELATIVE DISPLACEMENT RESPONSE TO BASE EXCITATION

By Tom Irvine  
Email: tomirvine@aol.com

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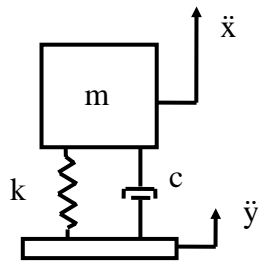
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## Introduction

The objective is to derive a Miles equation which gives the overall relative displacement response of a single-degree-of-freedom system to an applied force, where the excitation is in the form of a random vibration acceleration power spectral density.

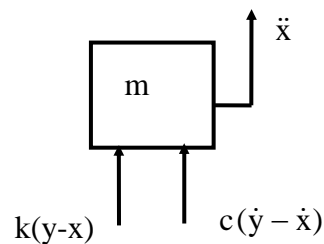
## Derivation

Consider a single degree-of-freedom system



where  $m$  equals mass,  $c$  equals the viscous damping coefficient, and  $k$  equals the stiffness. The absolute displacement of the mass equals  $x$ , and the base input displacement equals  $y$ .

The free-body diagram is



Summation of forces in the vertical direction,

$$\sum F = m\ddot{x} \quad (1)$$

$$m\ddot{x} = c(\dot{y} - \dot{x}) + k(y - x) \quad (2)$$

Substituting the relative displacement terms into equation (2) yields

$$m(\ddot{z} + \ddot{y}) = -c\dot{z} - kz \quad (3)$$

$$m\ddot{z} + c\dot{z} + kz = -m\ddot{y} \quad (4)$$

Dividing through by mass yields,

$$\ddot{z} + (c/m)\dot{z} + (k/m)z = -\ddot{y} \quad (5)$$

By convention,

$$(c/m) = 2\xi\omega_n$$

$$(k/m) = \omega_n^2$$

where  $\omega_n$  is the natural frequency in (radians/sec), and  $\xi$  is the damping ratio.

$$\ddot{z} + 2\xi\omega_n \dot{z} + \omega_n^2 z = -\ddot{y} \quad (6)$$

Let

$$z(t) = \hat{Z} \exp(j\omega t) \quad (7)$$

$$y(t) = \hat{Y} \exp(j\omega t) \quad (8)$$

$$\left[ -\omega^2 + j2\xi\omega\omega_n + \omega_n^2 \right] \hat{Z} \exp(j\omega t) = -\hat{Y} \exp(j\omega t) \quad (9)$$

Take the Fourier transform of each side.

$$\left[ -\omega^2 + j2\xi\omega\omega_n + \omega_n^2 \right] Z(\omega) = -Y(\omega) \quad (10)$$

$$Z(\omega) = \frac{-Y(\omega)}{\left[ -\omega^2 + \omega_n^2 + j2\xi\omega\omega_n \right]} \quad (11)$$

$$Z(f) = \frac{-(1/2\pi)Y(f)}{\left[ -f^2 + f_n^2 + j2\xi f f_n \right]} \quad (12)$$

Divide through by  $f_n^2$ .

$$Z(f) = \frac{-\left(1/(2\pi f_n)^2\right) Y(f)}{\left[ -\rho^2 + 1 + j2\xi\rho \right]} \quad (13)$$

where  $\rho = f/f_n$

$$Z(f) = \frac{-\left(1/(2\pi f_n)^2\right) Y(f)}{\left[ 1 - \rho^2 + j2\xi\rho \right]} \quad (14)$$

Multiply each side by its complex conjugate.

$$Z(f)Z^*(f) = \frac{\left(1/(2\pi f_n)^2\right)}{\left[ 1 - \rho^2 + j2\xi\rho \right]} \frac{\left(1/(2\pi f_n)^2\right)}{\left[ 1 - \rho^2 - j2\xi\rho \right]} Y(f)Y^*(f) \quad (15)$$

$$Z(f)Z^*(f) = \frac{\left(1/(2\pi f_n)^2\right)}{\left[ \rho^2 - 1 + j2\xi\rho \right]} \frac{\left(1/(2\pi f_n)^2\right)}{\left[ \rho^2 - 1 - j2\xi\rho \right]} Y(f)Y^*(f) \quad (16)$$

The transfer function  $H(\rho)$  times its complex conjugate is

$$H(\rho)H^*(\rho) = \left[ \frac{\left( \frac{1}{(2\pi f_n)^2} \right)}{\rho^2 - j2\xi\rho - 1} \right] \left[ \frac{\left( \frac{1}{(2\pi f_n)^2} \right)}{\rho^2 + j2\xi\rho - 1} \right] \quad (17)$$

Solve for the roots R1 and R2 of the first denominator.

$$R1, R2 = \frac{j2\xi \pm \sqrt{(-j2\xi)^2 - 4(-1)}}{2} \quad (18)$$

$$R1, R2 = \frac{j2\xi \pm \sqrt{-4\xi^2 + 4}}{2} \quad (19)$$

$$R1, R2 = j\xi \pm \sqrt{1 - \xi^2} \quad (20)$$

Solve for the roots R3 and R4 of the second denominator.

$$R3, R4 = \frac{-j\xi \pm \sqrt{(j2\xi)^2 - 4(-1)}}{2} \quad (21)$$

$$R3, R4 = \frac{-j2\xi \pm \sqrt{-4\xi^2 + 4}}{2} \quad (22)$$

$$R3, R4 = -j\xi \pm \sqrt{1 - \xi^2} \quad (23)$$

$$(24)$$

Summary,

$$R1 = +j\xi + \sqrt{1 - \xi^2} \quad (25)$$

$$R2 = +j\xi - \sqrt{1 - \xi^2} \quad (26)$$

$$R3 = -j\xi + \sqrt{1 - \xi^2} \quad (27)$$

$$R4 = -j\xi - \sqrt{1 - \xi^2} \quad (28)$$

Note

$$R2 = -R1^* \quad (29)$$

$$R3 = R1^* \quad (30)$$

$$R4 = -R1^* \quad (31)$$

Now substitute into the denominators.

$$H(\rho)H^*(\rho) = \left[ \frac{1/(2\pi f_n)^4}{\left(\rho - j\xi - \sqrt{1 - \xi^2}\right)\left(\rho - j\xi + \sqrt{1 - \xi^2}\right)\left(\rho + j\xi - \sqrt{1 - \xi^2}\right)\left(\rho + j\xi + \sqrt{1 - \xi^2}\right)} \right] \quad (32)$$

$$H(\rho)H^*(\rho) = \left[ \frac{1/(2\pi f_n)^4}{(\rho - R1)(\rho - R2)(\rho - R3)(\rho - R4)} \right] \quad (33)$$

$$H(\rho)H^*(\rho) = \left[ \frac{1/(2\pi f_n)^4}{(\rho - R1)(\rho + R1^*)(\rho - R1^*)(\rho + R1)} \right] \quad (34)$$

Expand into partial fractions.

$$\left[ \frac{1}{(\rho - R1)(\rho + R1^*)(\rho - R1^*)(\rho + R1)} \right] = \begin{aligned} &+ \frac{\alpha}{(\rho - R1)} \\ &+ \frac{\beta}{(\rho - R1^*)} \\ &+ \frac{\lambda}{(\rho + R1^*)} \\ &+ \frac{\sigma}{(\rho + R1)} \end{aligned} \quad (35)$$

Equation (35) is solved using the method in Reference 1.

$$\begin{bmatrix} \alpha \\ \beta \\ \lambda \\ \sigma \end{bmatrix} = \frac{1}{\begin{bmatrix} 8\xi\sqrt{1-\xi^2} \end{bmatrix}} \begin{bmatrix} -\xi - j\sqrt{1-\xi^2} \\ -\xi + j\sqrt{1-\xi^2} \\ +\xi - j\sqrt{1-\xi^2} \\ +\xi + j\sqrt{1-\xi^2} \end{bmatrix} \quad (36)$$

Let

$$\psi = \frac{\xi}{\sqrt{1-\xi^2}} \quad (37)$$

$$\begin{bmatrix} \alpha \\ \beta \\ \lambda \\ \sigma \end{bmatrix} = \frac{1}{8\xi} \begin{bmatrix} -\psi - j \\ -\psi + j \\ +\psi - j \\ +\psi + j \end{bmatrix} \quad (38)$$

$$R1 = +j\xi + \sqrt{1 - \xi^2} \quad (39)$$

$$\begin{aligned} \left[ \frac{1}{(\rho - R1)(\rho + R1^*)(\rho - R1^*)(\rho + R1)} \right] = & + \frac{-\psi - j}{\left( \rho - \sqrt{1 - \xi^2} - j\xi \right)} \left[ \frac{1}{8\xi} \right] \\ & + \frac{-\psi + j}{\left( \rho - \sqrt{1 - \xi^2} + j\xi \right)} \left[ \frac{1}{8\xi} \right] \\ & + \frac{+\psi - j}{\left( \rho + \sqrt{1 - \xi^2} - j\xi \right)} \left[ \frac{1}{8\xi} \right] \\ & + \frac{+\psi + j}{\left( \rho + \sqrt{1 - \xi^2} + j\xi \right)} \left[ \frac{1}{8\xi} \right] \end{aligned} \quad (40)$$

The overall relative displacement is found by integration.

$$[z_{\text{RMS}}(f_n, \xi)]^2 = \int_0^\infty H(\rho)H^*(\rho) \hat{Y}_{\text{APSD}}(f) df \quad (41)$$

$$[z_{\text{RMS}}(f_n, \xi)]^2 = f_n \int_0^\infty H(\rho)H^*(\rho) \hat{Y}_{\text{APSD}}(f) d\rho \quad (42)$$

Assume that the acceleration PSD is constant

$$\hat{Y}_{\text{APSD}}(f) = A \quad (43)$$

$$[x_{\text{RMS}}(f_n, \xi)]^2 = A f_n \int_0^\infty H(\rho)H^*(\rho) d\rho \quad (44)$$

$$\begin{aligned}
\{x_{\text{RMS}}(f_n, \xi)\}^2 \left[ \frac{8\xi (2\pi)^4 f_n^3}{A} \right] = & + \int_0^\infty \frac{-\psi - j}{\left( \rho - \sqrt{1 - \xi^2} - j\xi \right)} d\rho \\
& + \int_0^\infty \frac{-\psi + j}{\left( \rho - \sqrt{1 - \xi^2} + j\xi \right)} d\rho \\
& + \int_0^\infty \frac{+\psi - j}{\left( \rho + \sqrt{1 - \xi^2} - j\xi \right)} d\rho \\
& + \int_0^\infty \frac{+\psi + j}{\left( \rho + \sqrt{1 - \xi^2} + j\xi \right)} d\rho
\end{aligned} \tag{45}$$

Equation (45) is solved using the method in Reference 1.

$$\{z_{\text{RMS}}(f_n, \xi)\}^2 \left[ \frac{8\xi (2\pi)^4 f_n^3}{A} \right] = 2\pi \tag{46}$$

$$\{z_{\text{RMS}}(f_n, \xi)\}^2 = \left[ \frac{\pi}{4\xi} \right] \frac{A}{(2\pi)^4 f_n^3} \tag{47}$$

$$z_{\text{RMS}}(f_n, \xi) = \sqrt{\frac{\pi A}{4\xi (2\pi)^4 f_n^3}} \tag{48}$$



The RMS relative displacement is finally

$$z_{\text{RMS}}(f_n, \xi) = \sqrt{\frac{A}{64\pi^3 \xi f_n^3}} \quad (49)$$

$$Q = \frac{1}{2\xi} \quad (50)$$

$$z_{\text{RMS}} = \sqrt{\frac{QA}{32\pi^3 f_n^3}} \quad (51)$$

Note that equation for the absolute acceleration response in Reference 2 is

$$\ddot{x}_{\text{GRMS}}(f_n, Q) = \sqrt{\left(\frac{\pi}{2}\right) f_n Q A} \quad (52)$$

Thus

$$\ddot{x}_{\text{GRMS}} = [2\pi f_n]^2 z_{\text{RMS}} \quad (53)$$

## References

1. T. Irvine, Derivation of Miles Equation for an Applied Force, Vibrationdata, 2008.
2. T. Irvine, Derivation of Miles Equation Revision D, Vibrationdata, 2008.