

TRANSVERSE VIBRATION OF A BEAM SIMPLY-SUPPORTED AT EACH END WITH BENDING, SHEAR, AND ROTARY INERTIA

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Variables

$y(x, t)$ = Transverse displacement

E = Elastic modulus

G = Shear modulus

I = Area moment of inertia

A = Cross-section area

r = Radius of gyration

k = Shear factor

ρ = Mass/volume

Equation of Motion

Consider the bending vibration of a beam including both shear and rotary inertia effects. Assume that the beam is uniform. The equations of motion is

$$a^2 \frac{\partial^4 y}{\partial x^4} + \frac{\partial^2 y}{\partial t^2} - r^2 \left[1 + \frac{E}{kG} \right] \frac{\partial^4 y}{\partial x^2 \partial t^2} + r^2 \frac{\rho}{kG} \frac{\partial^4 y}{\partial t^4} = 0 \quad (1)$$

where

$$a^2 = \frac{EI}{\rho A} \quad (2)$$

$$r^2 = \frac{I}{A} \quad (3)$$

Assume that the displacement can be separated into spatial and temporal variables.

$$y(x, t) = Y(x)T(t) \quad (4)$$

$$a^2 Y''''(x)T(t) + Y(x)T''(t) - r^2 \left[1 + \frac{E}{kG} \right] Y''(x)T''(t) + r^2 \frac{\rho}{kG} Y(x)T''''(t) = 0 \quad (5)$$

$$a^2 \frac{Y''''(x)}{Y(x)} + \frac{T''(t)}{T(t)} - r^2 \left[1 + \frac{E}{kG} \right] \frac{Y''(x)T''(t)}{Y(x)T(t)} + r^2 \frac{\rho}{kG} \frac{T''''(t)}{T(t)} = 0 \quad (6)$$

Assume that the temporal function can be represented as

$$T(t) = A_n \cos \omega_n t + B_n \sin \omega_n t \quad (7)$$

$$T'(t) = \omega_n \{ -A_n \sin \omega_n t + B_n \cos \omega_n t \} \quad (8)$$

$$T''(t) = \omega_n^2 \{ -A_n \cos \omega_n t - B_n \sin \omega_n t \} \quad (9)$$

$$T'''(t) = \omega_n^3 \{ A_n \sin \omega_n t - B_n \cos \omega_n t \} \quad (10)$$

$$T''''(t) = \omega_n^4 \{ A_n \cos \omega_n t + B_n \sin \omega_n t \} \quad (11)$$

Note that

$$\frac{T''(t)}{T(t)} = -\omega_n^2 \quad (12)$$

$$\frac{T''''(t)}{T(t)} = \omega_n^4 \quad (13)$$

By substitution,

$$a^2 \frac{Y''''(x)}{Y(x)} - \omega_n^2 + \omega_n^2 r^2 \left[1 + \frac{E}{kG} \right] \frac{Y''(x)}{Y(x)} + \omega_n^4 r^2 \frac{\rho}{kG} = 0 \quad (14)$$

$$a^2 Y''''(x) + \omega_n^2 r^2 \left[1 + \frac{E}{kG} \right] Y''(x) + \omega_n^4 r^2 \frac{\rho}{kG} Y(x) - \omega_n^2 Y(x) = 0 \quad (15)$$

$$a^2 Y''''(x) + \omega_n^2 r^2 \left[1 + \frac{E}{kG} \right] Y''(x) + \omega_n^2 \left[\omega_n^2 r^2 \frac{\rho}{kG} - 1 \right] Y(x) = 0 \quad (16)$$

Assume a displacement function

$$Y(x) = a_1 \sinh(\beta x) + a_2 \cosh(\beta x) + a_3 \sin(\beta x) + a_4 \cos(\beta x) \quad (17)$$

$$\frac{dY(x)}{dx} = a_1 \beta \cosh(\beta x) + a_2 \beta \sinh(\beta x) + a_3 \beta \cos(\beta x) - a_4 \beta \sin(\beta x) \quad (18)$$

$$\frac{d^2 Y(x)}{dx^2} = a_1 \beta^2 \sinh(\beta x) + a_2 \beta^2 \cosh(\beta x) - a_3 \beta^2 \sin(\beta x) - a_4 \beta^2 \cos(\beta x) \quad (19)$$

$$\frac{d^3 Y(x)}{dx^3} = a_1 \beta^3 \cosh(\beta x) + a_2 \beta^3 \sinh(\beta x) - a_3 \beta^3 \cos(\beta x) + a_4 \beta^3 \sin(\beta x) \quad (20)$$

$$\frac{d^4 Y(x)}{dx^4} = a_1 \beta^4 \sinh(\beta x) + a_2 \beta^4 \cosh(\beta x) + a_3 \beta^4 \sin(\beta x) + a_4 \beta^4 \cos(\beta x) \quad (21)$$

APPENDIX A

Simply-Supported

The boundary conditions at the left end $x = 0$ are

$$Y(0) = 0 \quad (\text{zero displacement}) \quad (\text{A-1})$$

$$\left. \frac{d^2 Y}{dx^2} \right|_{x=0} = 0 \quad (\text{zero bending moment}) \quad (\text{A-2})$$

The boundary conditions at the free end $x = L$ are

$$Y(L) = 0 \quad (\text{zero displacement}) \quad (\text{A-3})$$

$$\left. \frac{d^2 Y}{dx^2} \right|_{x=L} = 0 \quad (\text{zero bending moment}) \quad (\text{A-4})$$

Apply boundary condition (A-1) to equation (17).

$$a_2 + a_4 = 0 \quad (\text{A-5})$$

$$a_4 = -a_2 \quad (\text{A-6})$$

Apply boundary condition (A-2) to equation (19).

$$a_2 - a_4 = 0 \quad (\text{A-7})$$

$$a_2 = a_4 \quad (\text{A-8})$$

Equations (A-7) and (A-8) can only be satisfied if

$$a_2 = 0 \quad (\text{A-9})$$

and

$$a_4 = 0 \quad (\text{A-10})$$

The spatial equations thus simplify to

$$Y(x) = a_1 \sinh(\beta x) + a_3 \sin(\beta x) \quad (A-11)$$

$$\frac{d^2 Y(x)}{dx^2} = a_1 \beta^2 \sinh(\beta x) - a_3 \beta^2 \sin(\beta x) \quad (A-12)$$

Apply boundary condition (A-6) to equation (17).

$$a_1 \sinh(\beta L) + a_3 \sin(\beta L) = 0 \quad (A-13)$$

Apply boundary condition (A-7) to equation (19).

$$a_1 \beta^2 \sinh(\beta L) - a_3 \beta^2 \sin(\beta L) = 0 \quad (A-14)$$

$$a_1 \sinh(\beta L) - a_3 \sin(\beta L) = 0 \quad (A-15)$$

$$\begin{bmatrix} \sinh(\beta L) & \sin(\beta L) \\ \sinh(\beta L) & -\sin(\beta L) \end{bmatrix} \begin{bmatrix} a_1 \\ a_3 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix} \quad (A-16)$$

By inspection, equation (A-19) can only be satisfied if $a_1 = 0$ and $a_3 = 0$. Set the determinant to zero in order to obtain a nontrivial solution.

$$-\sin(\beta L) \sinh(\beta L) - \sin(\beta L) \sinh(\beta L) = 0 \quad (A-17)$$

$$-2 \sin(\beta L) \sinh(\beta L) = 0 \quad (A-18)$$

$$\sin(\beta L) \sinh(\beta L) = 0 \quad (A-19)$$

Equation (A-19) is satisfied if

$$\beta_n L = n\pi, \quad n = 1, 2, 3, \dots \quad (A-20)$$

$$\beta_n = \frac{n\pi}{L}, \quad n = 1, 2, 3, \dots \quad (A-21)$$

The displacement function is

$$Y(x) = \hat{a}_1 \{ \sin(\beta L) \sinh(\beta x) + \sinh(\beta L) \sin(\beta x) \} \quad (A-22)$$

$$Y'(x) = \hat{a}_1 \beta \{ \sin(\beta L) \cosh(\beta x) + \sinh(\beta L) \cos(\beta x) \} \quad (A-23)$$

$$Y''(x) = \hat{a}_1 \beta^2 \{ \sin(\beta L) \sinh(\beta x) - \sinh(\beta L) \sin(\beta x) \} \quad (A-24)$$

$$Y'''(x) = \hat{a}_1 \beta^3 \{ \sin(\beta L) \cosh(\beta x) - \sinh(\beta L) \cos(\beta x) \} \quad (A-25)$$

$$Y''''(x) = \hat{a}_1 \beta^4 \{ \sin(\beta L) \sinh(\beta x) + \sinh(\beta L) \sin(\beta x) \} \quad (A-26)$$

$$\begin{aligned} & a^2 \hat{a}_1 \beta^4 \{ \sin(\beta L) \sinh(\beta x) + \sinh(\beta L) \sin(\beta x) \} \\ & + \omega_n^2 r^2 \left[1 + \frac{E}{kG} \right] \hat{a}_1 \beta^2 \{ \sin(\beta L) \sinh(\beta x) - \sinh(\beta L) \sin(\beta x) \} \\ & + \omega_n^2 \left[\omega_n^2 r^2 \frac{\rho}{kG} - 1 \right] \hat{a}_1 \{ \sin(\beta L) \sinh(\beta x) + \sinh(\beta L) \sin(\beta x) \} = 0 \end{aligned} \quad (A-27)$$

$$\begin{aligned} & a^2 \left\{ \frac{n\pi}{L} \right\}^4 \{ \sin(n\pi) \sinh(n\pi x/L) + \sinh(n\pi) \sin(n\pi x/L) \} \\ & + \omega_n^2 r^2 \left[1 + \frac{E}{kG} \right] \left\{ \frac{n\pi}{L} \right\}^2 \{ \sin(n\pi) \sinh(n\pi x/L) - \sinh(n\pi) \sin(n\pi x/L) \} \\ & + \omega_n^2 \left[\omega_n^2 r^2 \frac{\rho}{kG} - 1 \right] \{ \sin(n\pi) \sinh(n\pi x/L) + \sinh(n\pi) \sin(n\pi x/L) \} = 0 \end{aligned} \quad (A-28)$$

$$\begin{aligned} & a^2 \left\{ \frac{n\pi}{L} \right\}^4 \{ \sinh(n\pi) \sin(n\pi x/L) \} + \omega_n^2 r^2 \left[1 + \frac{E}{kG} \right] \left\{ \frac{n\pi}{L} \right\}^2 \{ -\sinh(n\pi) \sin(n\pi x/L) \} \\ & + \omega_n^2 \left[\omega_n^2 r^2 \frac{\rho}{kG} - 1 \right] \{ \sinh(n\pi) \sin(n\pi x/L) \} = 0 \end{aligned} \quad (A-29)$$

$$a^2 \left\{ \frac{n\pi}{L} \right\}^4 - \omega_n^2 r^2 \left[1 + \frac{E}{kG} \right] \left\{ \frac{n\pi}{L} \right\}^2 + \omega_n^2 \left[\omega_n^2 r^2 \frac{\rho}{kG} - 1 \right] = 0 \quad (\text{A-30})$$

$$a^2 \left\{ \frac{n\pi}{L} \right\}^4 - \omega_n^2 r^2 \left[1 + \frac{E}{kG} \right] \left\{ \frac{n\pi}{L} \right\}^2 + \omega_n^4 r^2 \frac{\rho}{kG} - \omega_n^2 = 0 \quad (\text{A-31})$$

$$a^2 \left[\frac{n\pi}{L} \right]^4 - \omega_n^2 \left\{ 1 + r^2 \left[1 + \frac{E}{kG} \right] \left[\frac{n\pi}{L} \right]^2 \right\} + \omega_n^4 r^2 \frac{\rho}{kG} = 0 \quad (\text{A-32})$$

Solve for ω_n ,

$$\omega_n^2 = \left\{ \frac{kG}{2r^2 \rho} \right\} \left\{ 1 + r^2 \left[1 + \frac{E}{kG} \right] \left[\frac{n\pi}{L} \right]^2 \pm \sqrt{\left\{ 1 + r^2 \left[1 + \frac{E}{kG} \right] \left[\frac{n\pi}{L} \right]^2 \right\}^2 - 4r^2 \frac{\rho}{kG} a^2 \left[\frac{n\pi}{L} \right]^4} \right\} \quad (\text{A-33})$$

$$\omega_n = \frac{1}{r} \sqrt{\left\{ \frac{kG}{2\rho} \right\} \left\{ 1 + r^2 \left[1 + \frac{E}{kG} \right] \left[\frac{n\pi}{L} \right]^2 \pm \sqrt{\left\{ 1 + r^2 \left[1 + \frac{E}{kG} \right] \left[\frac{n\pi}{L} \right]^2 \right\}^2 - 4r^2 \frac{\rho}{kG} a^2 \left[\frac{n\pi}{L} \right]^4} \right\}} \quad (\text{A-34})$$

Note the shear modulus can be expressed as

$$G = \frac{E}{2(1+\nu)} \quad (\text{A-35})$$

where ν is the Poisson's ratio.

Recall

$$a^2 = \frac{EI}{\rho A} \quad (\text{A-36})$$

$$r^2 = \frac{I}{A} \quad (\text{A-37})$$

References

1. Weaver, Timoshenko, and Young; Vibration Problems in Engineering, Wiley-Interscience, New York, 1990.
2. T. Irvine, Application of the Newton-Raphson Method to Vibration Problems, Vibrationdata Publications, 1999.