

Structural-Acoustics Tutorial

Part 1 - Fundamentals

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Overview

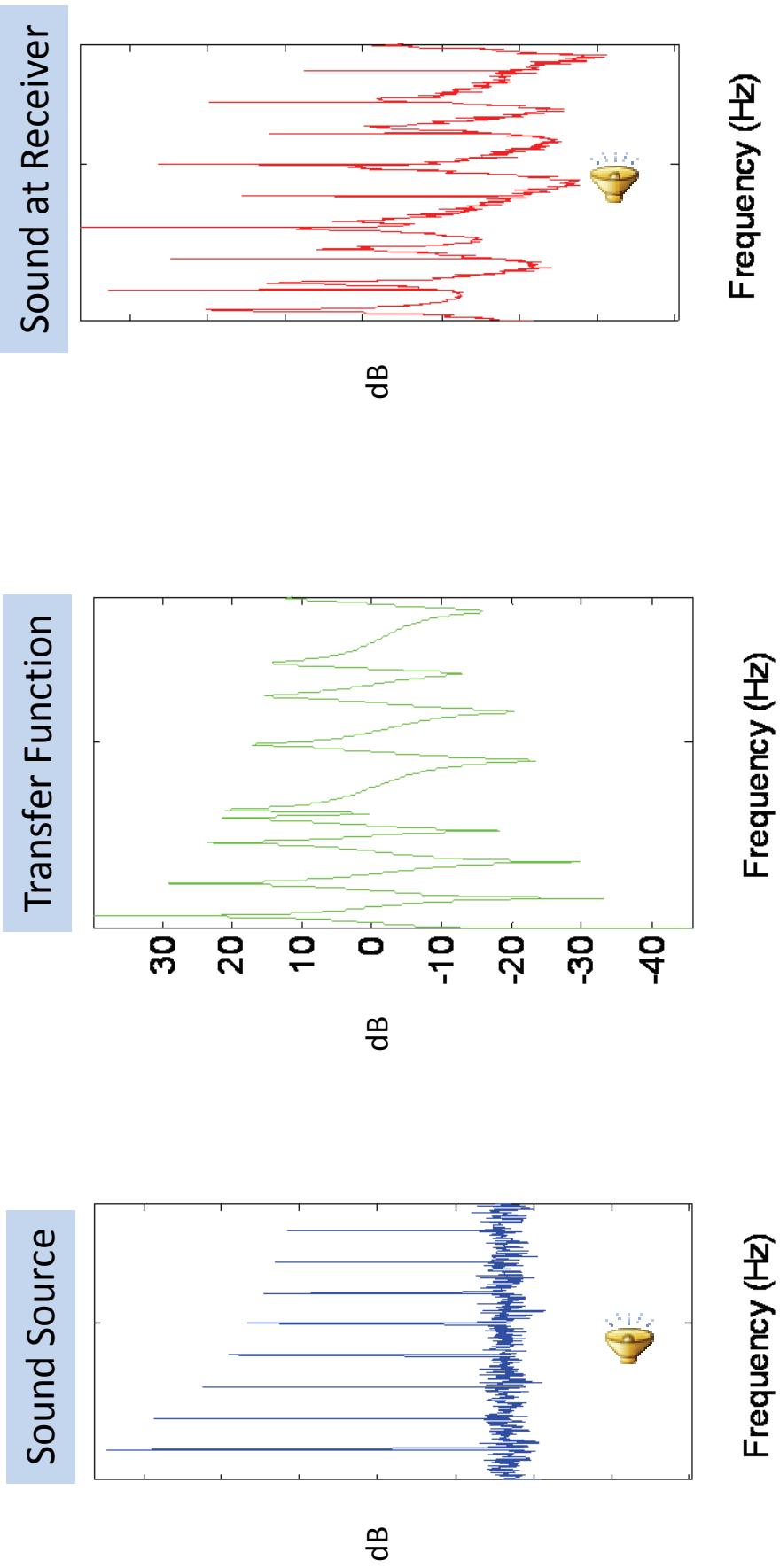
- Instructor
- Structural Vibrations
 - Modes in beams and plates
 - Mobility
- Sound radiated by structural waves
 - Radiation efficiency
- Structural waves generated by impinging sound
 - Transmission loss
- Brief introduction to numerical methods
 - FE, BE, SEA

Instructor

- Dr. Stephen A. Hambric
 - Applied Research Lab, Penn State University
 - Also Professor in Penn States' Graduate Program in Acoustics
 - Associate Director, Penn State Center for Acoustics and Vibration (CAV)
- Accompanying materials:
 - Structural Acoustics Tutorials, Parts 1 and 2, from *Acoustics Today* magazine
 - Download at www.hambricacoustics.com

Motivation

- Structures can amplify (and attenuate) sound sources substantially



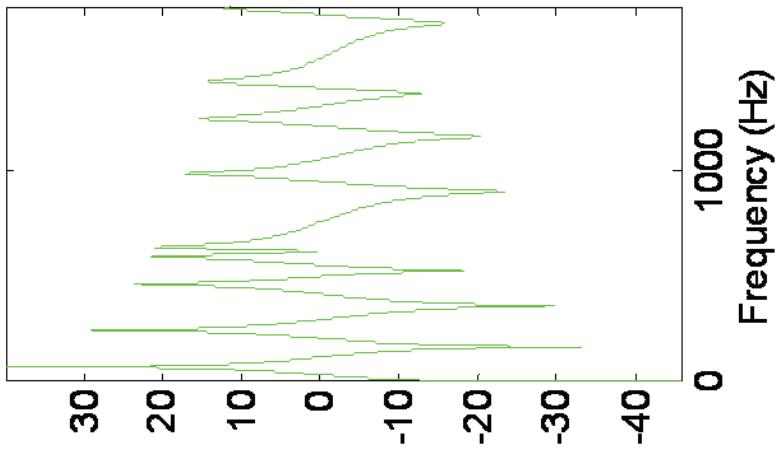
Structural Acoustic Transfer Functions

- Define transfer function:

$$\frac{P_{rad}}{\bar{F}^2} \longleftrightarrow \frac{\text{Sound power}}{\text{Applied force}^2}$$

- How is it defined?

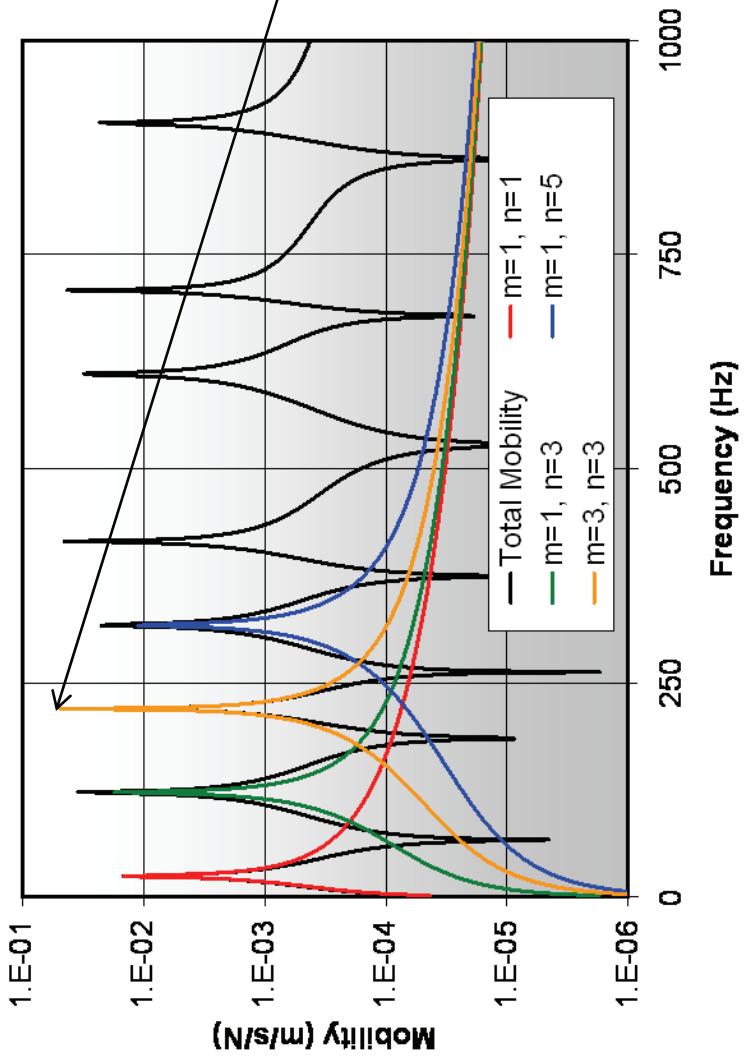
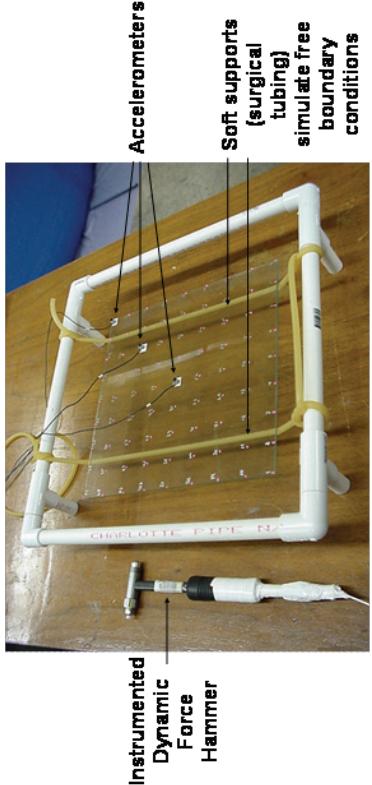
$$\frac{P_{rad}}{\bar{F}^2} = \frac{\langle |\bar{v}|^2 \rangle}{\bar{F}^2} \frac{P_{rad}}{\rho_o c_o A \langle |\bar{v}|^2 \rangle} \left[\begin{array}{l} \text{Fluid impedance} \\ \text{Sound power radiation efficiency} \\ \text{Surface averaged mobility} \end{array} \right]$$



Surface Averaged Mobility

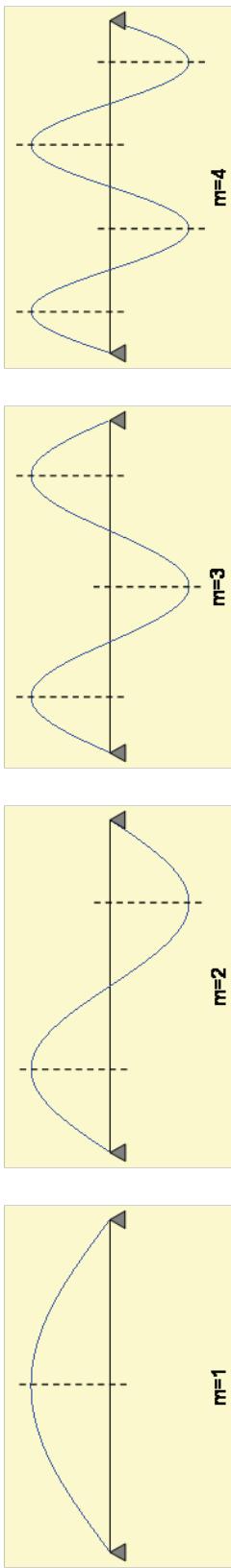
$$\left\langle \frac{|\bar{v}|^2}{\bar{F}^2} \right\rangle$$

- Averaged surface vibration amplitudes caused by known forces (mobilities)



Modes of Resonance

- Superposition of forward and backward traveling waves
- Example for flexure of simply supported beam:



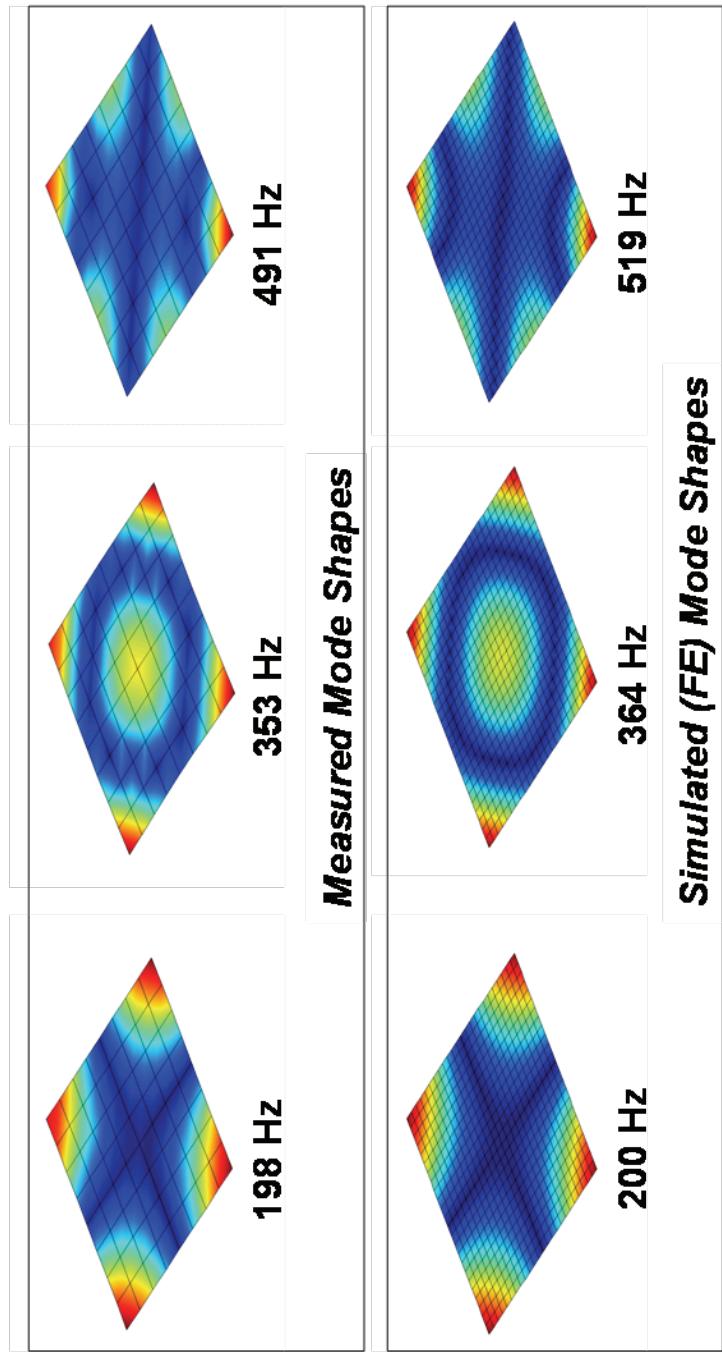
$$\omega_m = k_m^2 \sqrt{\frac{EI}{\rho A}} = \frac{m^2 \pi^2}{a^2} \sqrt{\frac{EI}{\rho A}}$$

- For other boundary conditions, wavenumbers change, e.g., for free boundaries:

$$\omega_m \approx \frac{\pi^2 (2m-1)^2}{4a^2} \sqrt{\frac{EI}{\rho A}}$$

Modes of Resonance

- Can also be computed with Finite Element (FE) models or measured
 - Measured and simulated resonance frequencies seldom match exactly



Mobility as a Summation of Modes

- A structure's mobility function is a simple series summation of modal responses to a driving force
 - Example: simply supported rectangular plate

$$\frac{v(x, y)}{F(x_o, y_o)} = \frac{i\omega}{\left(\frac{\rho h a b}{4}\right)} \times \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} \left(\frac{1}{\omega_{mn}^2 - \omega^2} \left[\sin \frac{m\pi x}{a} \sin \frac{n\pi y}{b} \right] \times \left[\sin \frac{m\pi x_0}{a} \sin \frac{n\pi y_0}{b} \right] \right)$$

Mode shape at drive location

Mode shape at response location

Difference between drive and resonance frequencies

Modal mass (fraction of static mass)

Modal Response Peaks

- Why isn't modal response infinite at resonance frequencies?

$$\frac{v(\textcolor{blue}{x}, \textcolor{blue}{y})}{F(\textcolor{violet}{x}_o, \textcolor{violet}{y}_o)} \propto \frac{1}{\omega_{mn}^2 - \omega^2}$$

- Because ω_{mn} is complex, due to damping
 - For lightly damped systems:

$$\omega_{mn} \cong \tilde{\omega}_{mn} \left(1 + i \frac{\eta}{2} \right)$$

where η is the loss factor

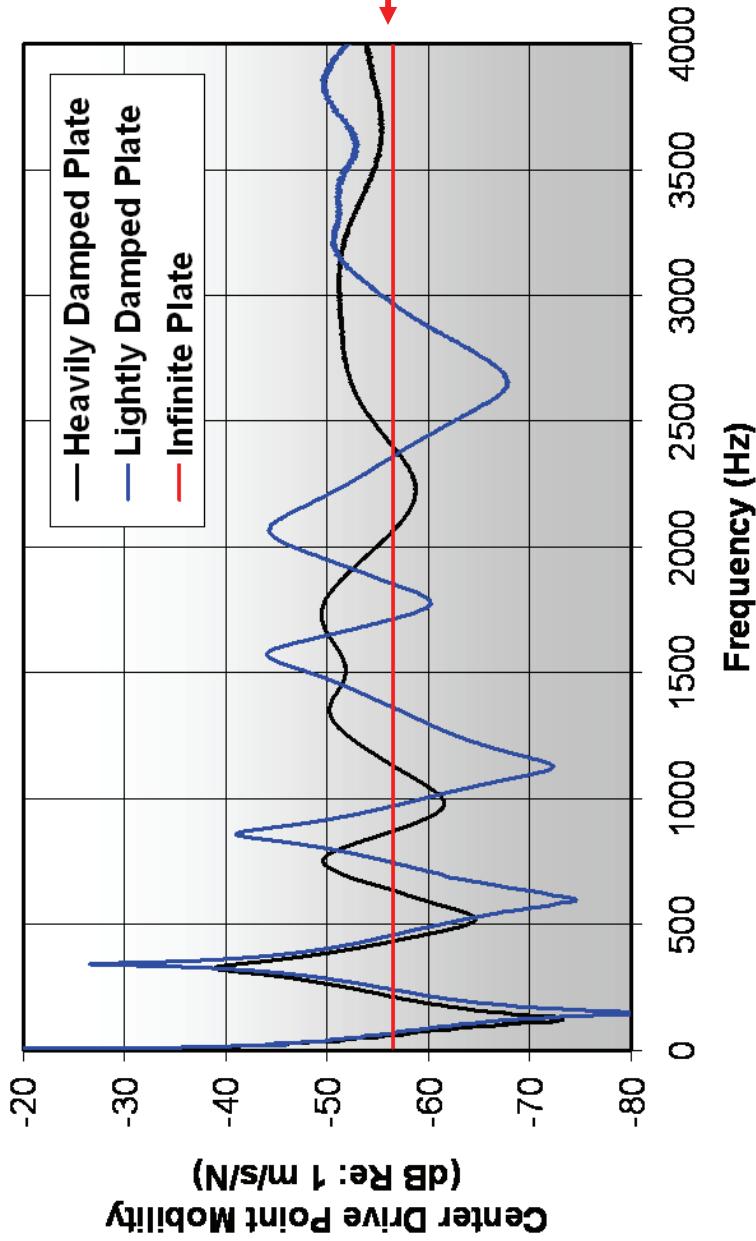
Damping Mechanisms



- Thin sheets of rubber adhered to the surface, or sandwiched between structures
- Adjoining structures
 - Coupling losses
 - Joint losses (friction)
- Sound radiation

Effects of Damping On Modal Response Peaks

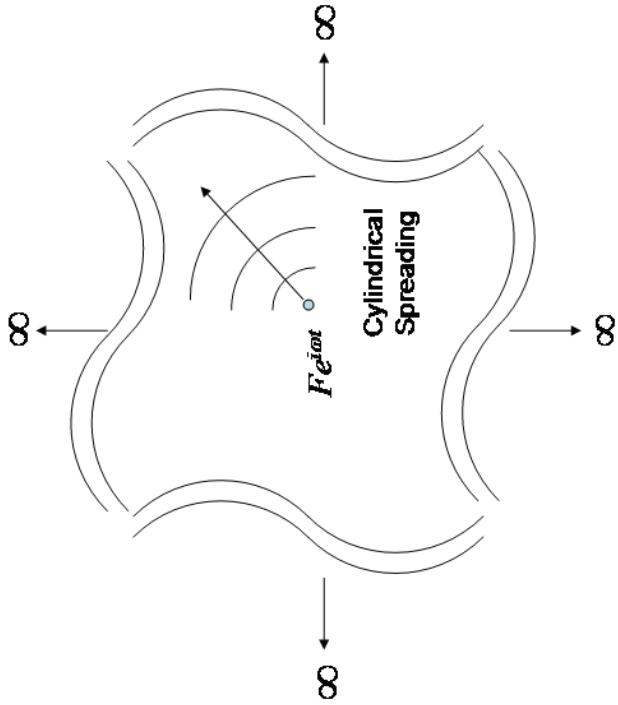
- Peak (and ‘anti-peak’) amplitudes decrease with increasing damping
 - Mobility approaches the mean levels of an infinite plate



How can mobility
of an infinite plate
be computed?

Infinite Structure Mobilities

- A structure is effectively infinite when waves reflected from boundaries are very weak with respect to the original waves emanating from a source

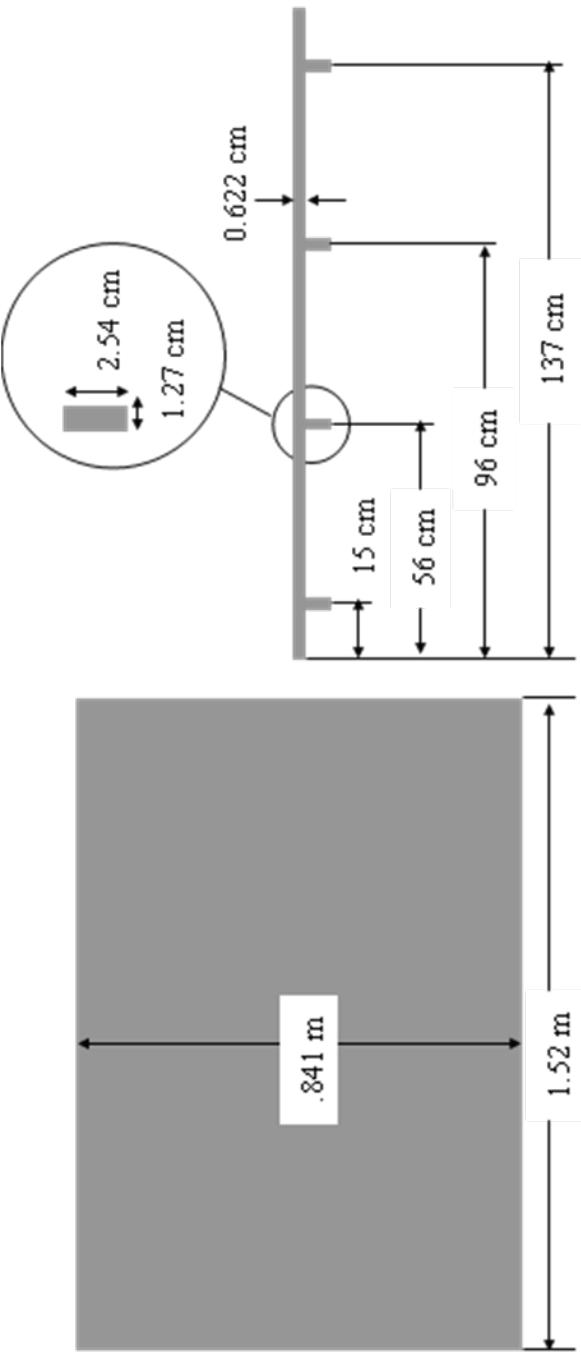


$$\text{For plates: } Y_{\inf} = (\nu / F)_{\inf} = \frac{1}{8\sqrt{D\rho h}}$$

- Useful for:
 - scaling mobilities
 - performing engineering estimates of proposed material changes
 - Checking mobility measurement accuracy

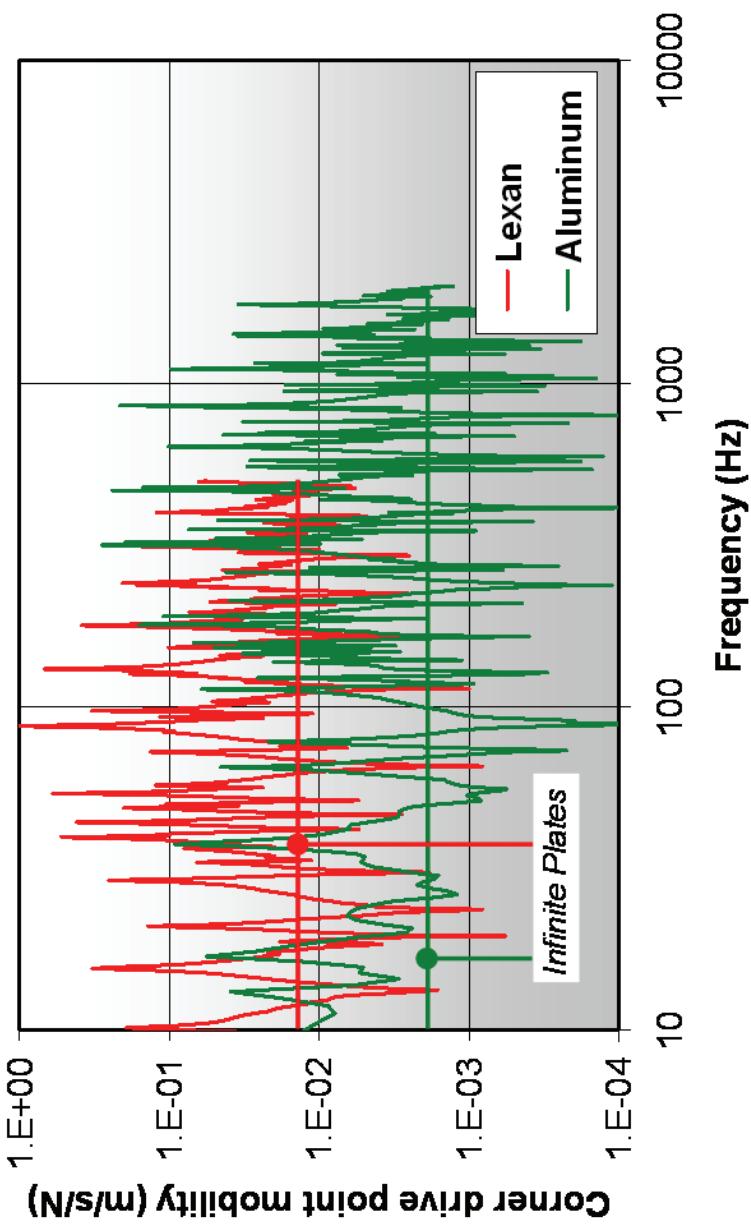
Infinite Structure Mobility Scaling Example

- Two panels with identical geometries and different materials
 - Lexan (plastic) and Aluminum



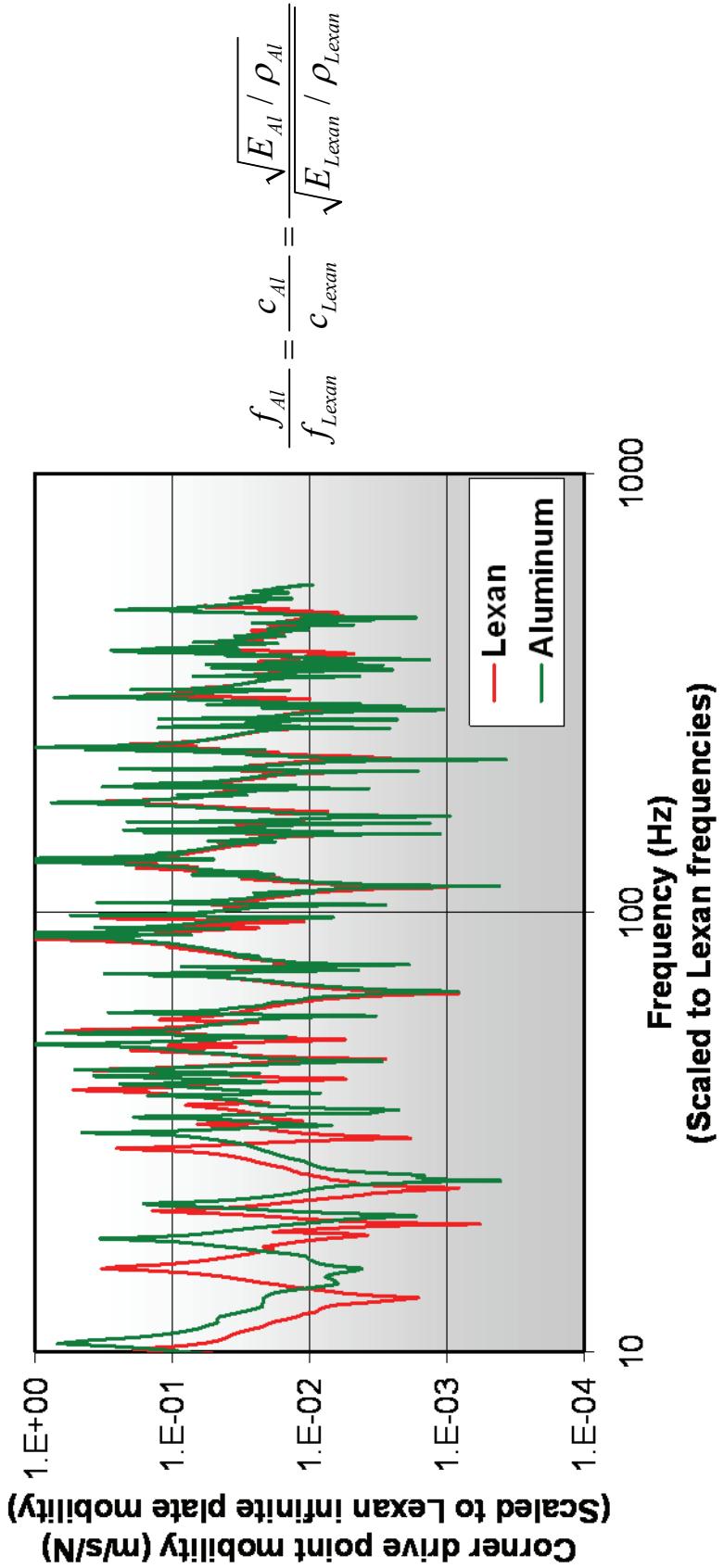
Infinite Structure Mobility Scaling Example

- Measured mobilities of both panels



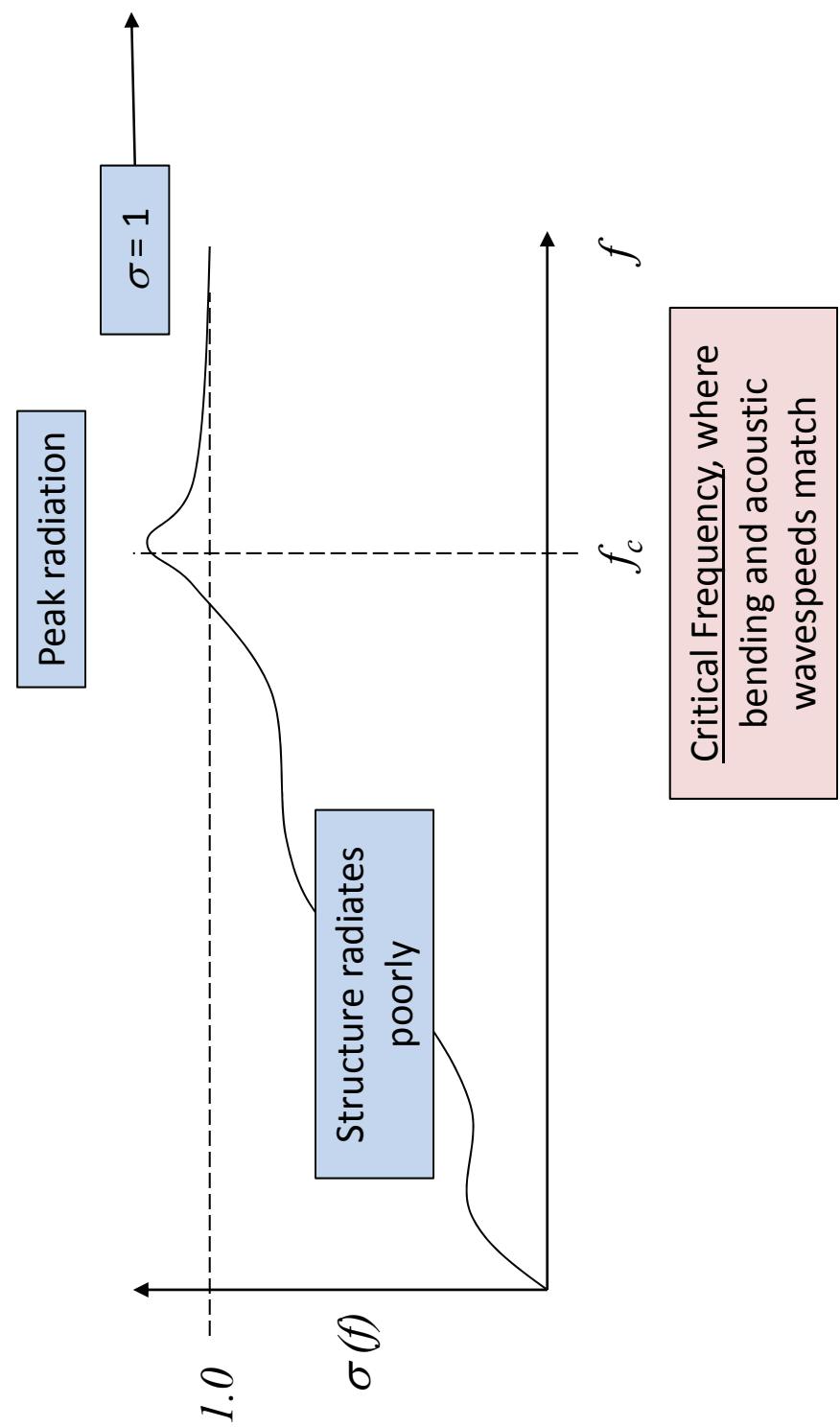
Infinite Structure Mobility Scaling Example

- Aluminum panel mobility scaled to that of Lexan

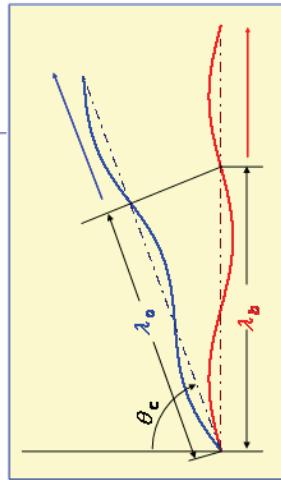
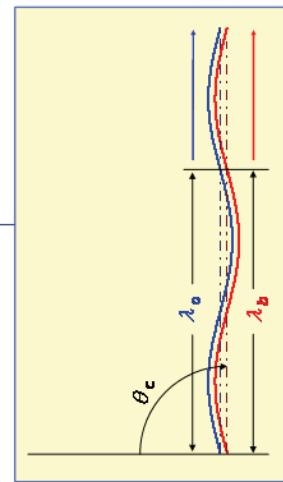
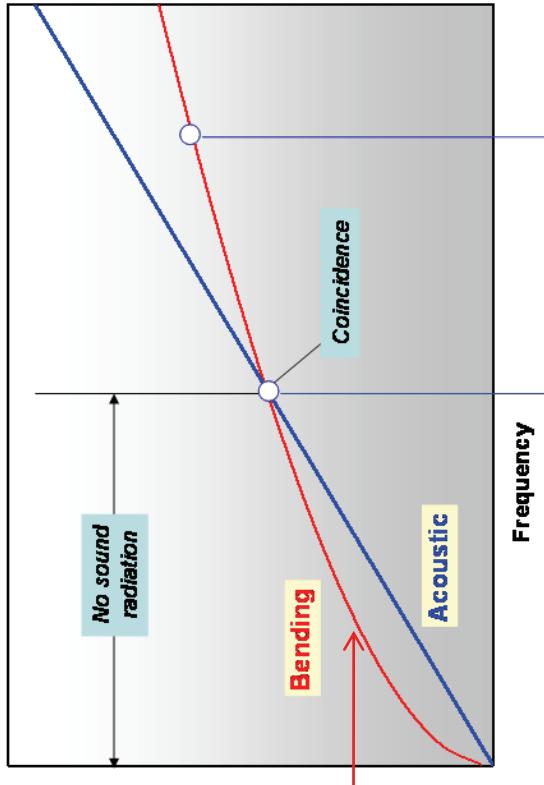


Radiation Efficiency

$$\frac{P_{rad}}{\rho_o c_o A \langle |\vec{v}|^2 \rangle}$$



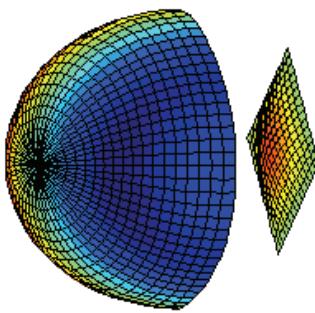
Coincidence



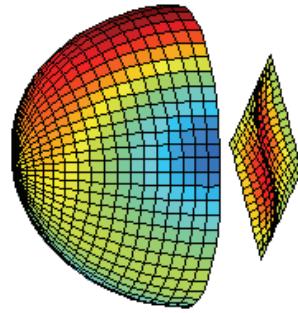
Bending waves are dispersive, slower than acoustic waves at low frequencies (subsonic), and faster at high frequencies (supersonic)

Radiating Flat Baffled Panel Below Coincidence

$$m = 1, n = 1, k_0/k_{mn} = 0.638$$

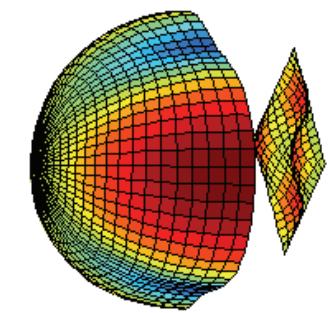


$$m = 1, n = 2, k_0/k_{mn} = 0.404$$

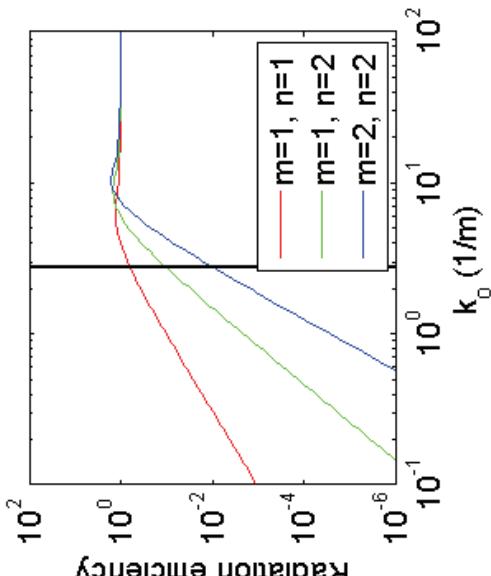


Pressures

$$m = 2, n = 2, k_0/k_{mn} = 0.319$$



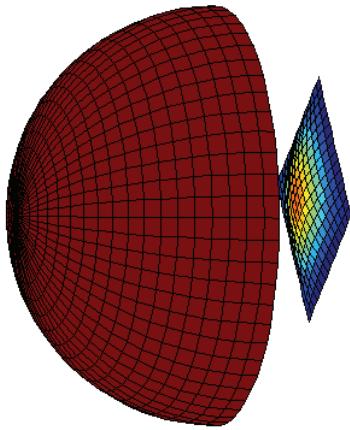
Radiation efficiency



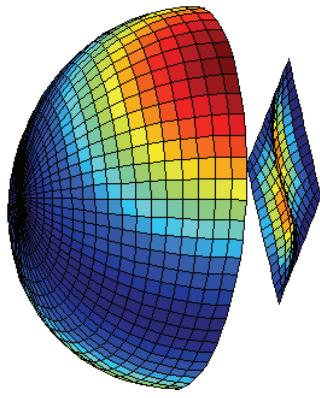
Odd/Odd >
Odd/Even >
Even/Even

Radiating Flat Baffled Panel – Increasing Frequency

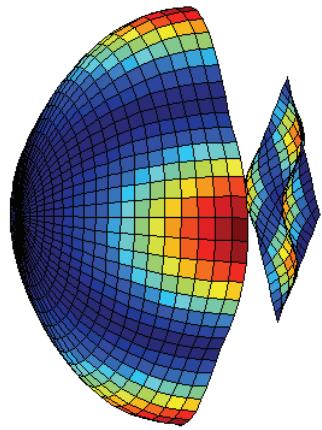
$$m = 1, n = 1, k_0/k_{mn} = 0.090$$



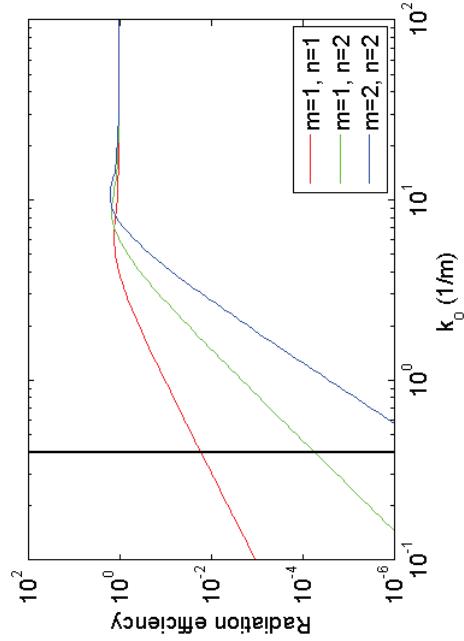
$$m = 1, n = 2, k_0/k_{mn} = 0.057$$



$$m = 2, n = 2, k_0/k_{mn} = 0.045$$

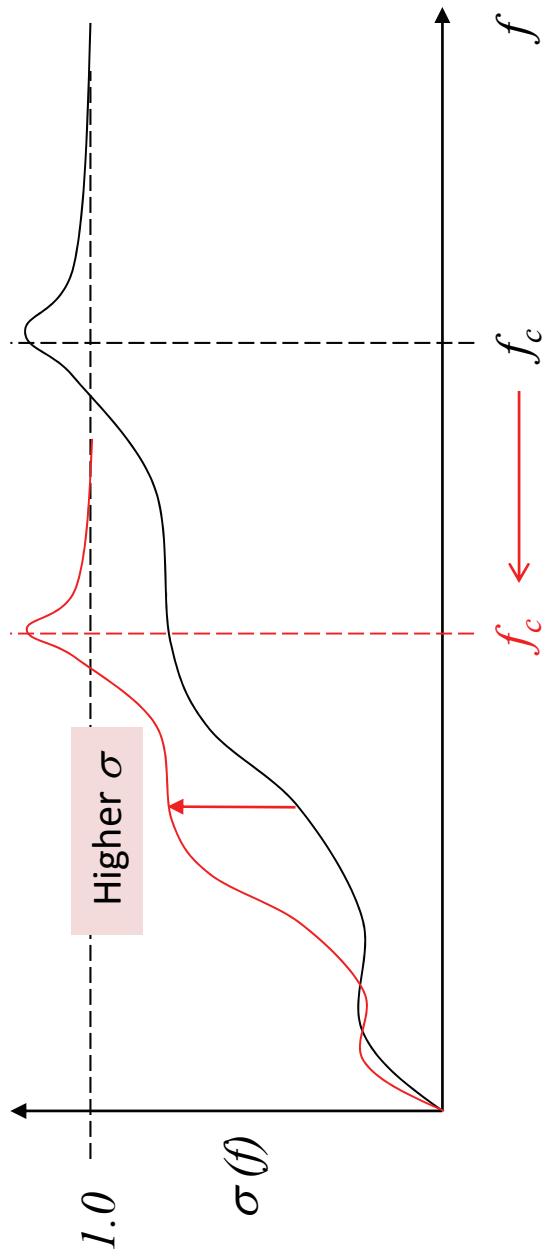


Intensities
(proportional
to square of
pressure)



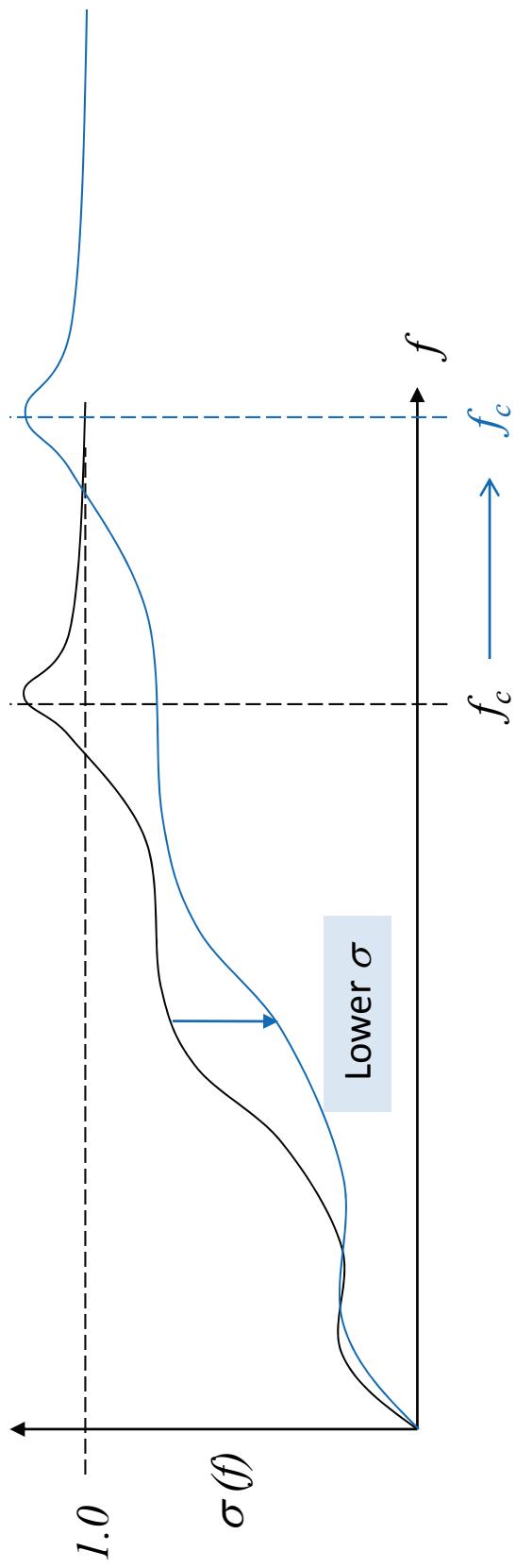
Radiation Efficiency – Effects of Coincidence Frequency Shifts

Stiffer, lighter
structure with
faster waves



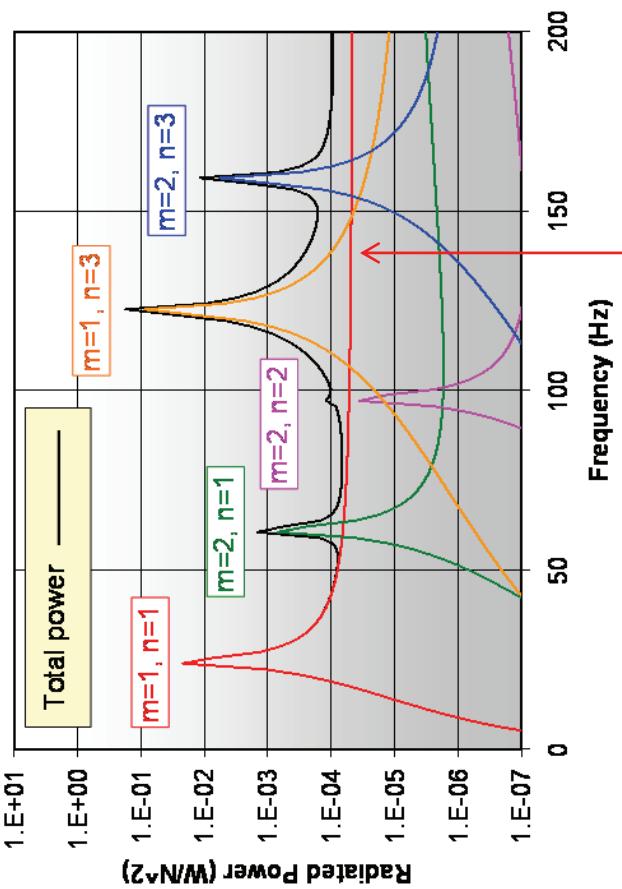
Radiation Efficiency – Effects Of Coincidence Frequency Shifts

Flimsier, heavier
structure with
slower waves

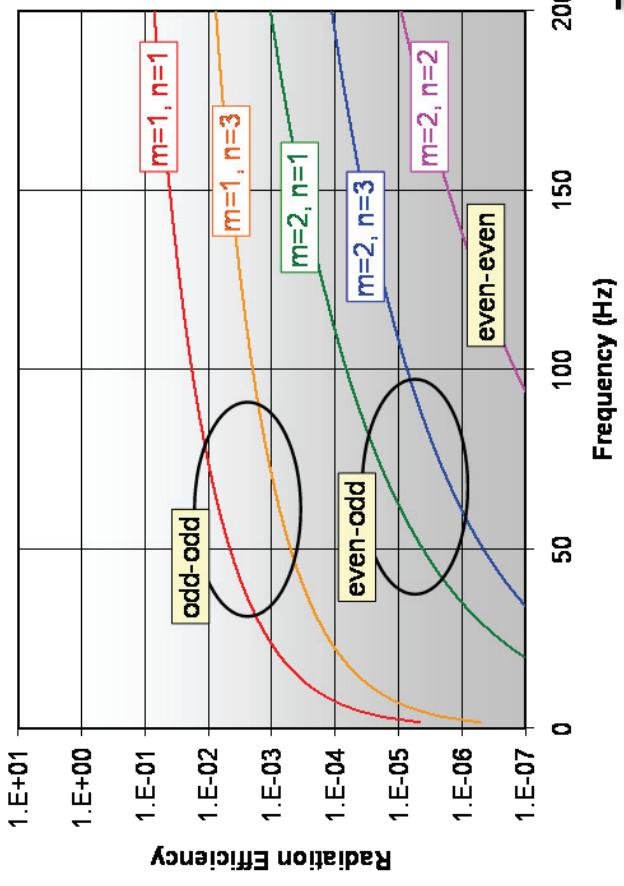
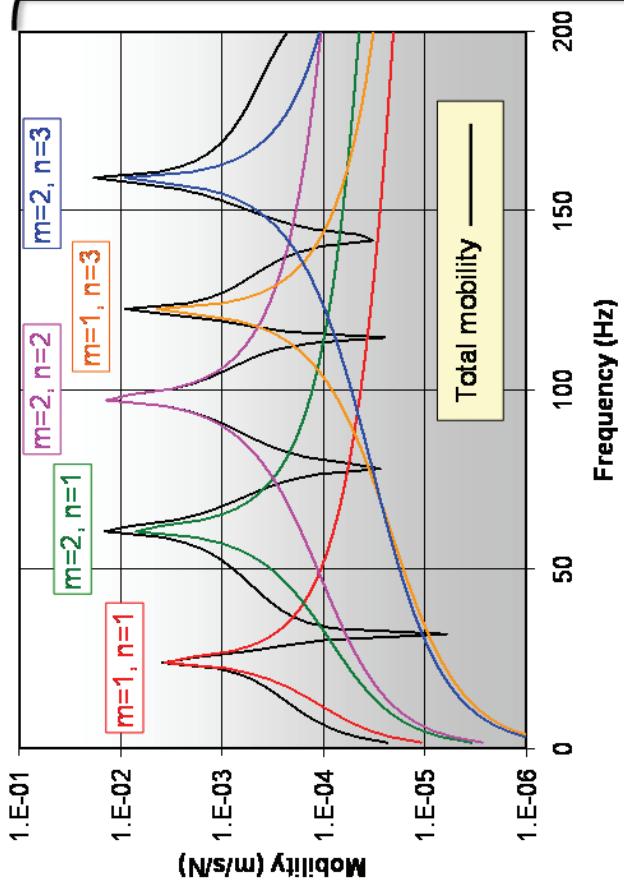


Sound Power Transfer Functions

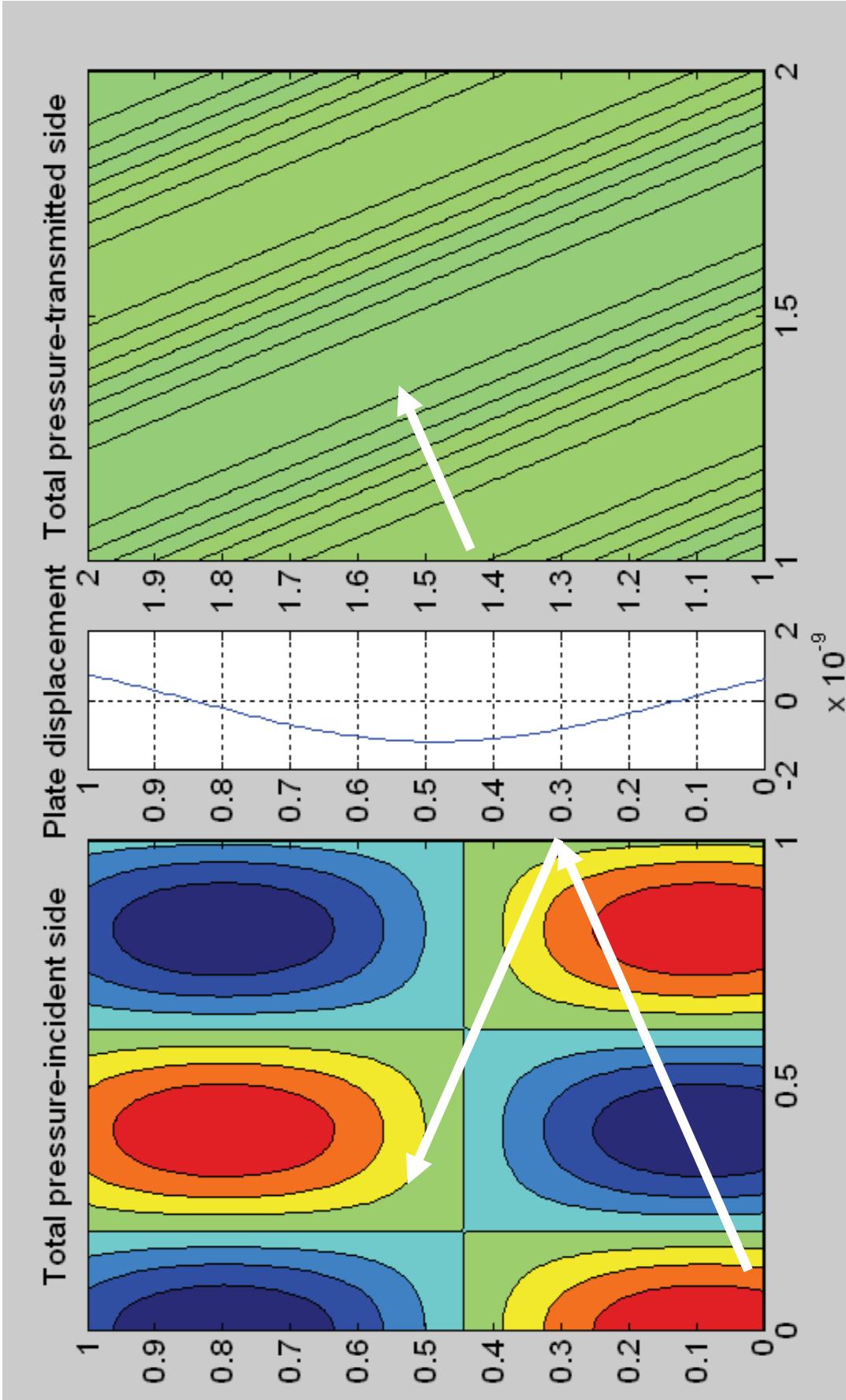
- Combining surface averaged mobility with radiation efficiency tells us how well a structure radiates sound when driven by a known force



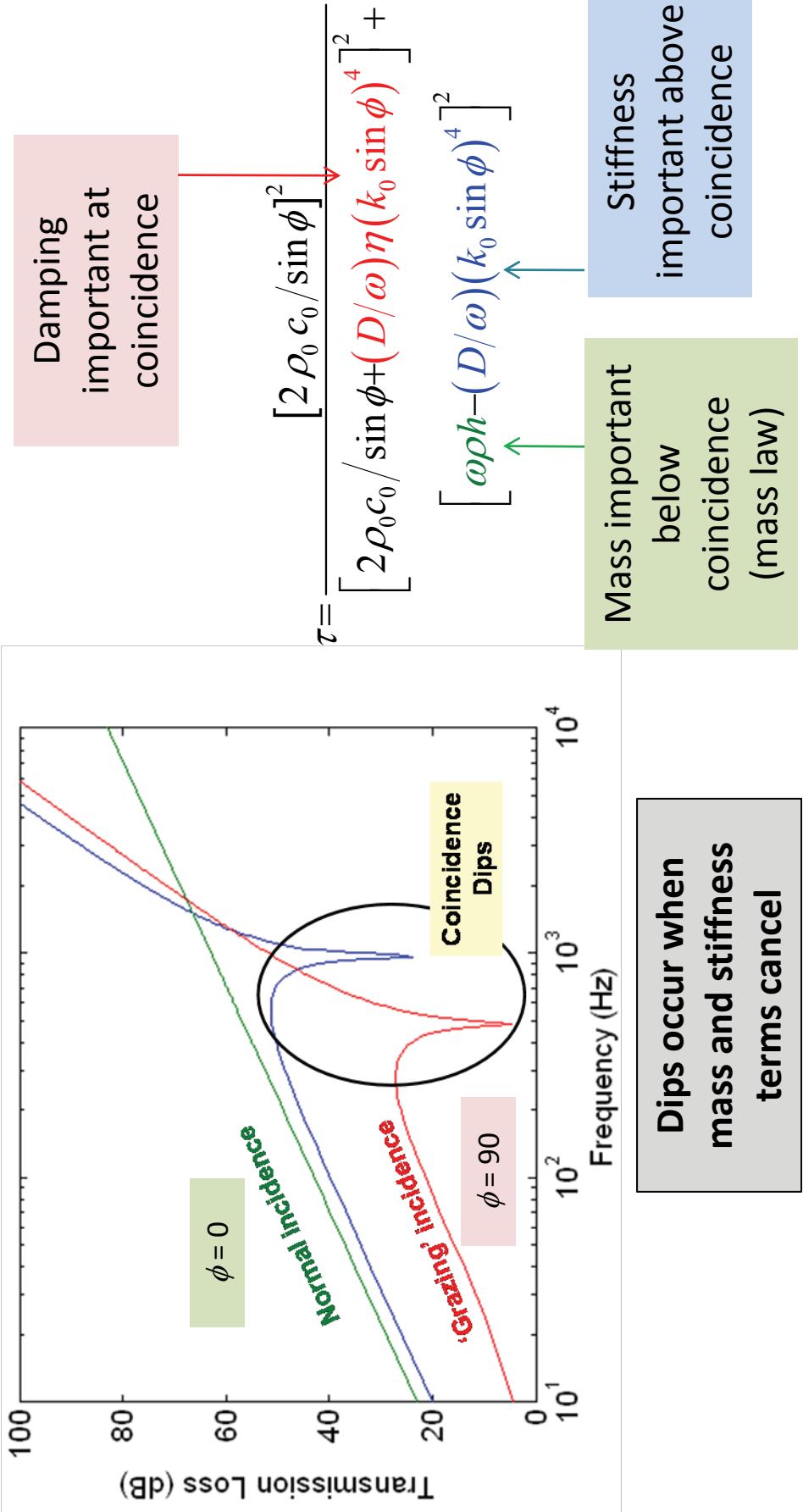
$(1,1)$ mode \rightarrow
'loudspeaker' mode



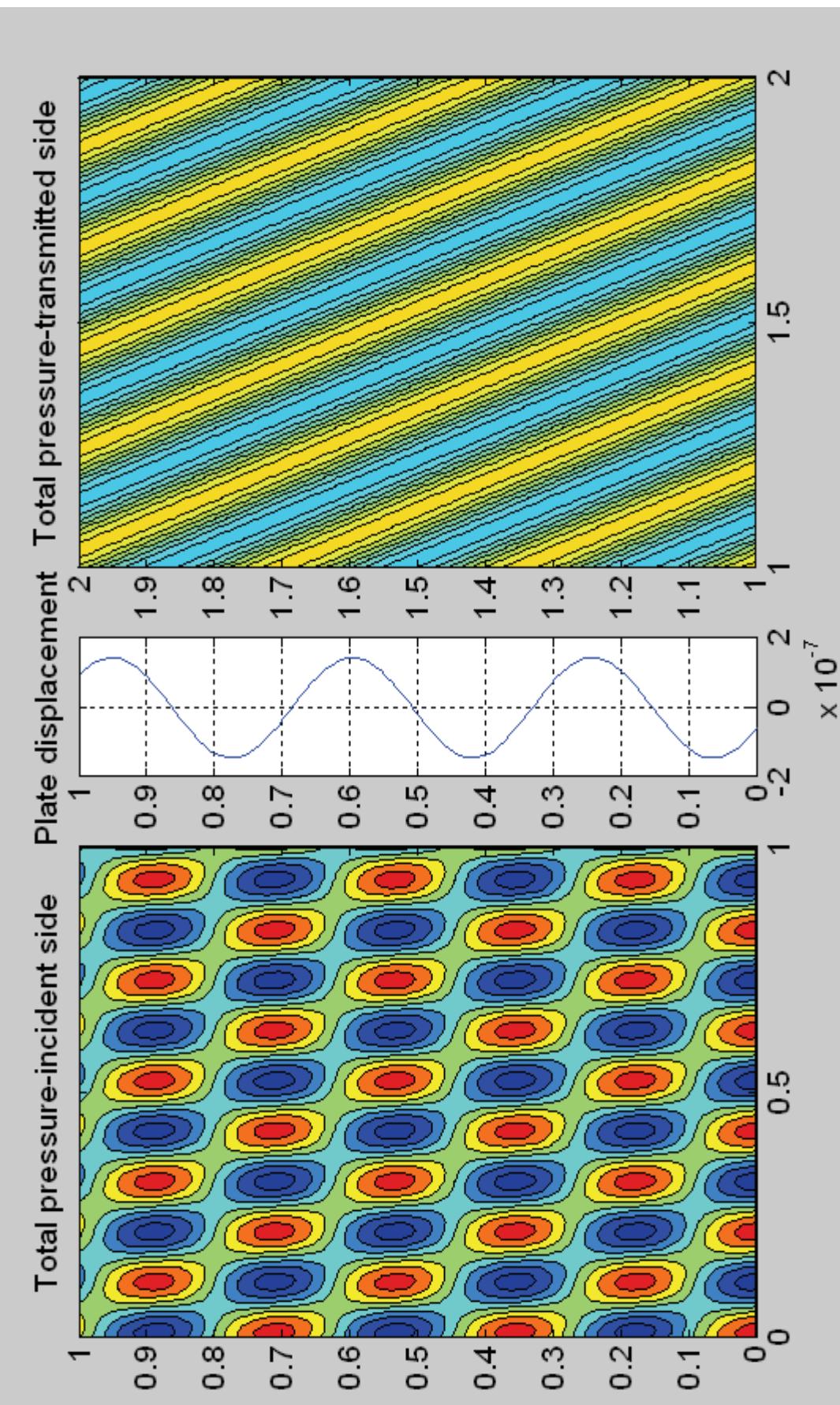
Acoustic Waves Impinging on Structures



Sound Transmission Loss of an Infinite Panel

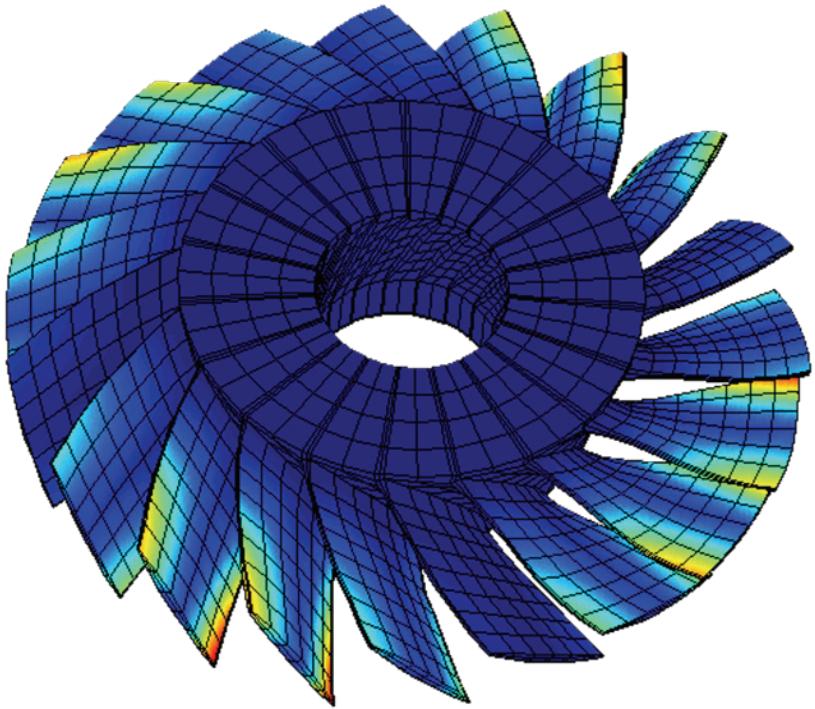


Sound Transmission near Coincidence

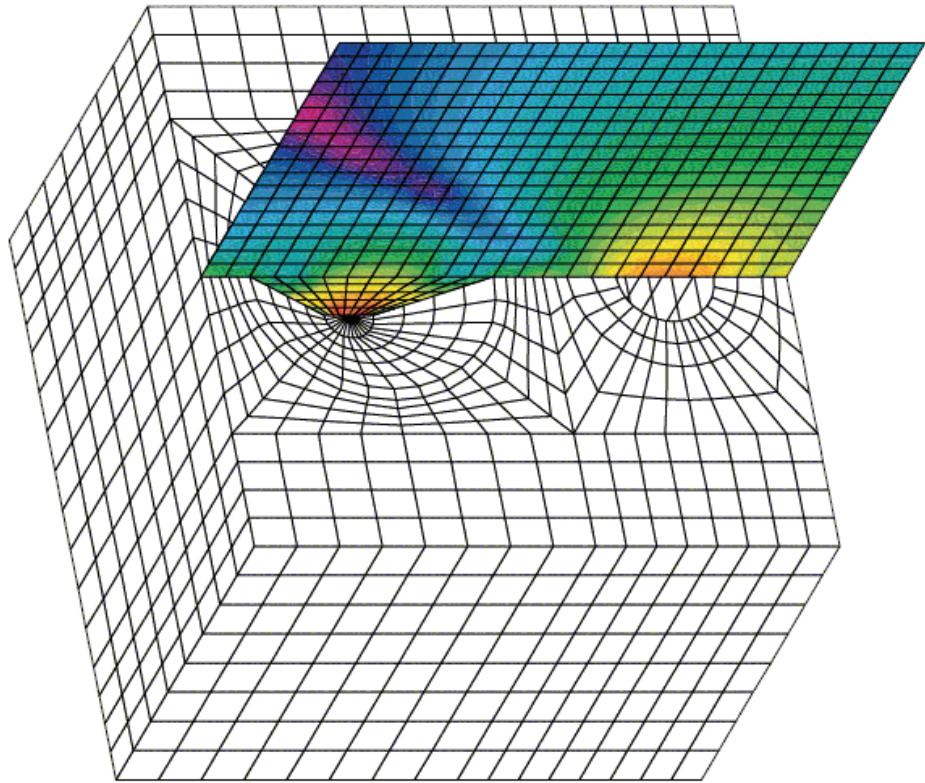


Finite Element (FE) Analysis

- Used generally to model structures
 - Plates, beams, and solids
- Also sometimes used to model acoustic regions, usually inside an object
- Many commercial software packages available



Boundary Element (BE) Analysis

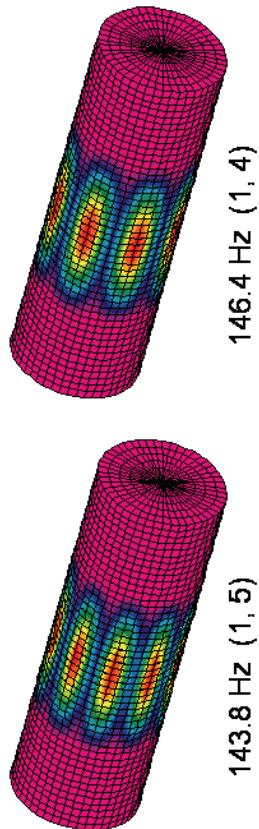


- Used to model the *boundaries* of acoustic regions
 - Inside or outside a vibrating surface
- Once surface pressures and velocities are known, the acoustic field anywhere may be computed
- Some commercial software packages are available (not as many as FE packages)

Coupled FE/BE Analyses

- Impedance matrices of structures (from FE) and acoustic regions (from BE) may be coupled
 - Enforce continuity of normal fluctuating velocity along boundary

		$\mathbf{f}_{\text{fluid}} / \mathbf{f}_{\text{in vacuo}}$						
Analysis Method	NA	(1,5)	(1,4)	(1,6)	(1,3)	(1,7)	(2,6)	(1,2)
Analytical	-	0.489	0.456	0.520	0.421	0.547	0.527	0.391
FE/BE	320	0.605	0.548	0.653	0.486	0.684	0.663	0.427
	720	0.545	0.498	0.589	0.448	0.629	0.601	0.401
	1440	0.491	0.455	0.523	0.418	0.553	0.538	0.382



Statistical Energy Analysis (SEA)

- SEA models the energy exchange between large groups of resonances in interconnected structures and acoustic regions
 - Usually used at high frequencies, where mode counts are very high
- Exchange of energy is modeled statistically
 - Get calculations averaged over large regions, and over wide frequency (usually one-third octave) bands
- Fast computations, independent of increasing frequency
- Va-One software