

# STEADY-STATE RELATIVE DISPLACEMENT RESPONSE TO BASE EXCITATION

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April 24, 2004

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## Introduction

Consider the single-degree-of-freedom system in Figure 1.

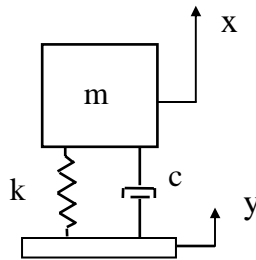


Figure 1.

where

- m is the mass
- c is the viscous damping coefficient
- k is the stiffness
- x is the absolute displacement of the mass
- y is the base input displacement

Newton's law can be applied to a free-body diagram of an individual system, as shown in Figure 2.

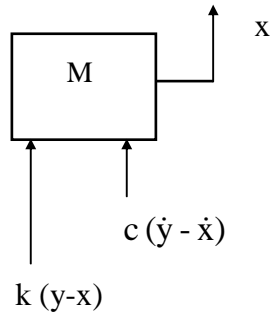


Figure 2. Free-body Diagram

A summation of forces yields the following governing differential equation of motion:

$$m \ddot{x} + c \dot{x} + kx = c \dot{y} + ky \quad (1)$$

A relative displacement can be defined as  $z = x - y$ .

The following equation is obtained by substituting this expression into equation (1):

$$m \ddot{z} + c \dot{z} + kz = -m \ddot{y} \quad (2)$$

Additional substitutions can be made as follows,

$$\omega_n^2 = \frac{k}{m} \quad (3)$$

$$2\xi \omega_n = \frac{c}{m} \quad (4)$$

Note that  $\xi$  is the damping ratio, and that  $\omega_n$  is the natural frequency in radians per second.

Furthermore,  $\xi$  is often represented by the amplification factor  $Q$ , where  $Q = 1/(2\xi)$ .

Substitution of these terms into equation (2) yields an equation of motion for the relative response

$$\ddot{z} + 2\xi\omega_n\dot{z} + \omega_n^2 z = -\ddot{y}(t) \quad (5)$$

Take the Fourier transform of both sides of equation (5).

$$\int_{-\infty}^{\infty} \left\{ \ddot{z}(t) + 2\xi\omega_n \dot{z}(t) + \omega_n^2 z(t) \right\} \exp[-j\omega t] dt = - \int_{-\infty}^{\infty} \ddot{y}(t) \exp[-j\omega t] dt \quad (6)$$

$$\begin{aligned} \int_{-\infty}^{\infty} \ddot{z}(t) \exp[-j\omega t] dt + 2\xi\omega_n \int_{-\infty}^{\infty} \dot{z}(t) \exp[-j\omega t] dt + \omega_n^2 \int_{-\infty}^{\infty} z(t) \exp[-j\omega t] dt \\ = - \int_{-\infty}^{\infty} \ddot{y}(t) \exp[-j\omega t] dt \end{aligned} \quad (7)$$

$$\int_{-\infty}^{\infty} \dot{z}(t) \exp[-j\omega t] dt = j\omega \int_{-\infty}^{\infty} z(t) \exp[-j\omega t] dt \quad (8)$$

$$\int_{-\infty}^{\infty} \ddot{z}(t) \exp[-j\omega t] dt = -\omega^2 \int_{-\infty}^{\infty} z(t) \exp[-j\omega t] dt \quad (9)$$

Substitute equations (8) and (9) into (7).

$$\begin{aligned}
& -\omega^2 \int_{-\infty}^{\infty} z(t) \exp[-j\omega t] dt + j2\xi\omega\omega_n \int_{-\infty}^{\infty} z(t) \exp[-j\omega t] dt + \omega_n^2 \int_{-\infty}^{\infty} z(t) \exp[-j\omega t] dt \\
& \qquad \qquad \qquad = - \int_{-\infty}^{\infty} \ddot{y}(t) \exp[-j\omega t] dt
\end{aligned} \tag{10}$$

$$\{(\omega_n^2 - \omega^2) + j2\xi\omega\omega_n\} \int_{-\infty}^{\infty} z(t) \exp[-j\omega t] dt = - \int_{-\infty}^{\infty} \ddot{y}(t) \exp[-j\omega t] dt \tag{11}$$

$$Z(\omega) = \int_{-\infty}^{\infty} z(t) \exp[-j\omega t] dt \tag{12}$$

$$\ddot{Y}(\omega) = \int_{-\infty}^{\infty} \ddot{y}(t) \exp[-j\omega t] dt \tag{13}$$

Substitute equations (12) and (13) into (11).

$$\{(\omega_n^2 - \omega^2) + j2\xi\omega\omega_n\} Z(\omega) = - \ddot{Y}(\omega) \tag{14}$$

$$\frac{Z(\omega)}{\ddot{Y}(\omega)} = \frac{-1}{\{(\omega_n^2 - \omega^2) + j2\xi\omega\omega_n\}} \tag{15}$$

The transfer function  $H(\omega)$  is

$$H(\omega) = \frac{Z(\omega)}{\ddot{Y}(\omega)} \tag{16}$$

$$H(\omega) = \frac{-1}{\{(\omega_n^2 - \omega^2) + j2\xi\omega\omega_n\}} \tag{17}$$

The transfer function magnitude is

$$|H(\omega)| = \frac{1}{\sqrt{(\omega_n^2 - \omega^2)^2 + (2\xi\omega\omega_n)^2}} \quad (18)$$

$$|H(f)| = \frac{1}{4\pi^2 \sqrt{(f_n^2 - f^2)^2 + (2\xi f f_n)^2}} \quad (19)$$

Recall

$$H(\omega) = \frac{-1}{\{(\omega_n^2 - \omega^2) + j2\xi\omega\omega_n\}} \quad (20)$$

Multiply the numerator and denominator by the complex conjugate of the denominator.

$$H(\omega) = -\frac{(\omega_n^2 - \omega^2) - j2\xi\omega\omega_n}{\{(\omega_n^2 - \omega^2)^2 + (2\xi\omega\omega_n)^2\}} \quad (21)$$

$$H(\omega) = \frac{(\omega^2 - \omega_n^2) + j2\xi\omega\omega_n}{\{(\omega_n^2 - \omega^2)^2 + (2\xi\omega\omega_n)^2\}} \quad (22)$$

The phase angle is

$$\phi = \arctan \left[ \frac{2\xi\omega\omega_n}{\omega^2 - \omega_n^2} \right] \quad (23)$$

$$\varphi = \arctan \left[ \frac{2\xi f f_n}{f^2 - f_n^2} \right] \quad (24)$$

Recall

$$|H(\omega)| = \frac{1}{\sqrt{(\omega_n^2 - \omega^2)^2 + (2\xi\omega\omega_n)^2}} \quad (25)$$

$$|H(\omega)| = \frac{1}{\omega_n^2 \sqrt{(1 - \rho^2)^2 + (2\xi\rho)^2}}$$

where  $\rho = \omega / \omega_n$

(26)

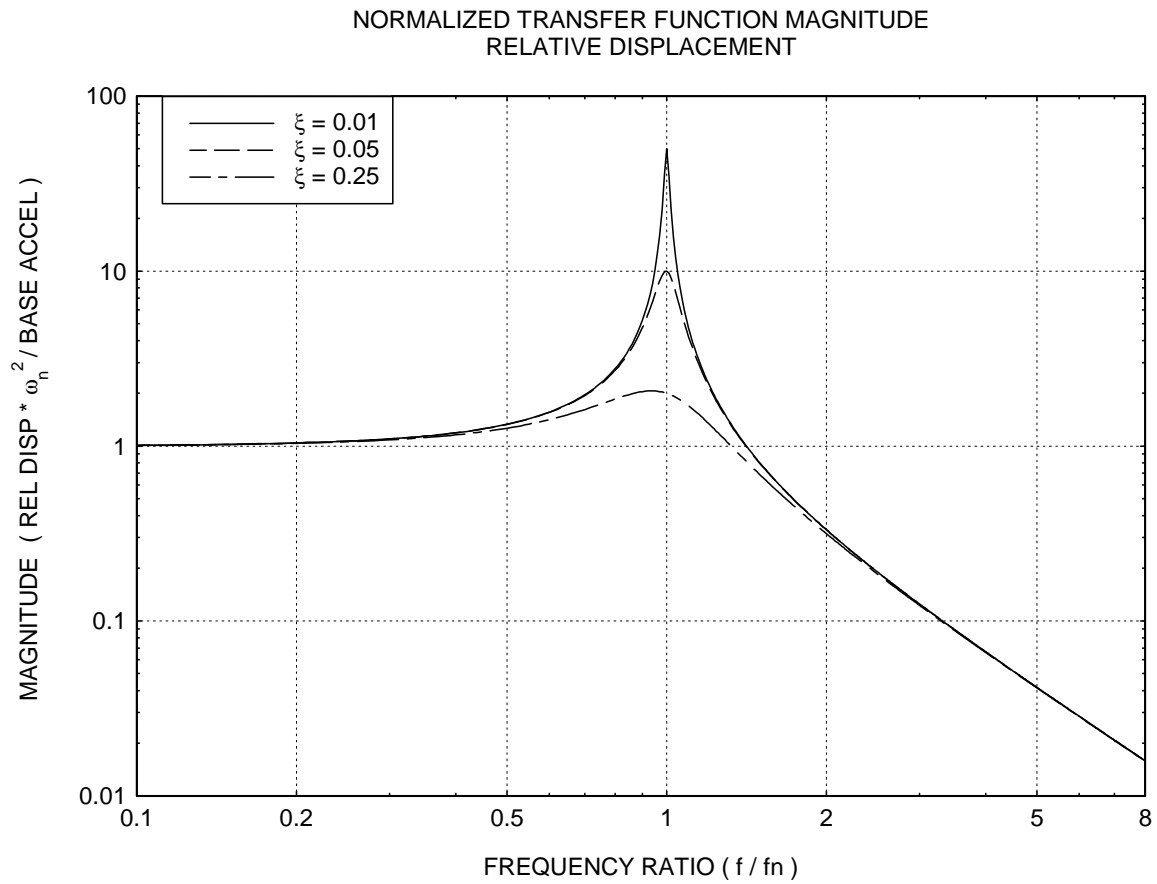


Figure 3.

Note that the units must be consistent. For example, acceleration must be in terms of  $\text{in}^2/\text{sec}$  if relative displacement is in terms of inches.

TRANSFER FUNCTION PHASE ANGLE  
RELATIVE DISPLACEMENT / BASE ACCELERATION

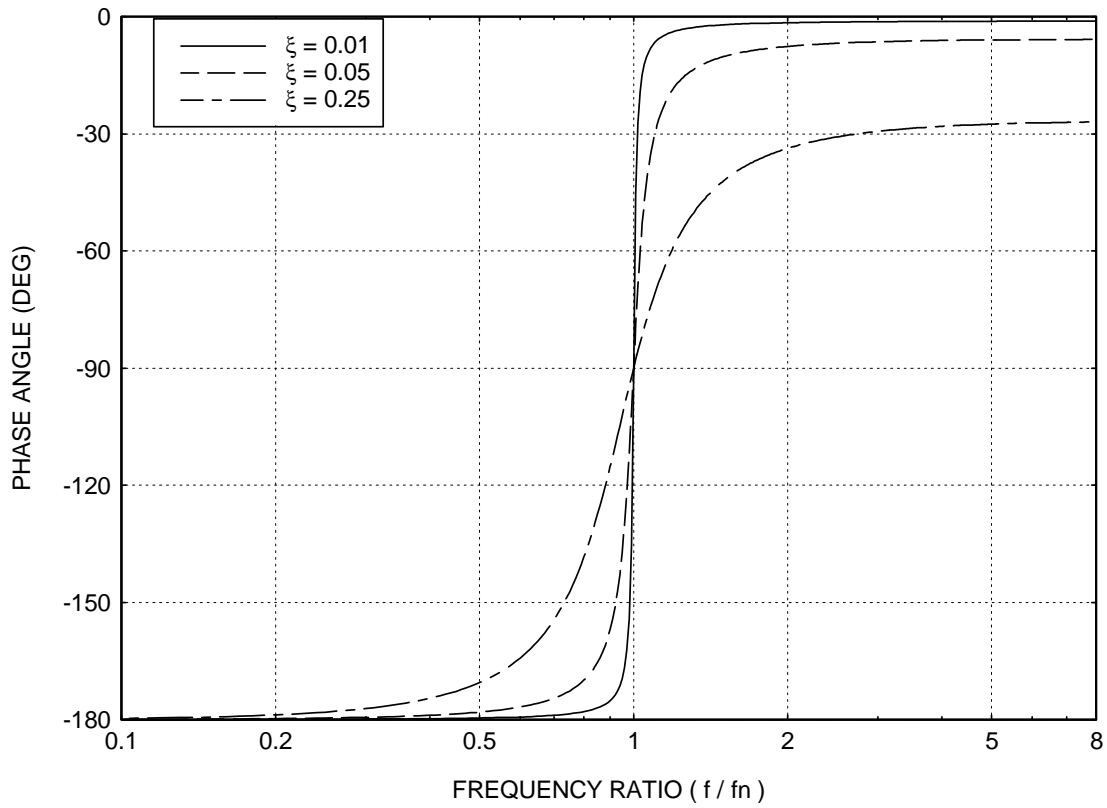


Figure 4.