



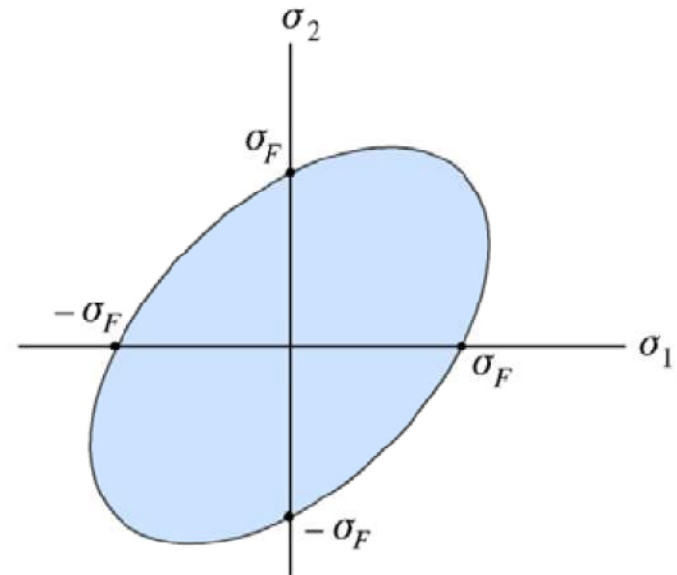
# Von Mises Stress PSD using MSC.Random

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- Introduction
- Calculation of PSD of von Mises stress
- Verification of MSC.Random results
- Application at a big model
  - Performance data
  - Typical results
  - Hints on problems and difficulties
- Conclusion

- Von Mises is the most widely used stress equivalent in static analysis
- Is valid for ductile materials
- Useable for 2-dimensional and 3-dimensional stress fields
- Typical parameter for durability analysis
- Customers often request it, also in multi-frequency dynamic analysis
- *For random analysis the standard von Mises formula gives wrong results*



- Under dynamic load the von Mises stress is not centered about zero

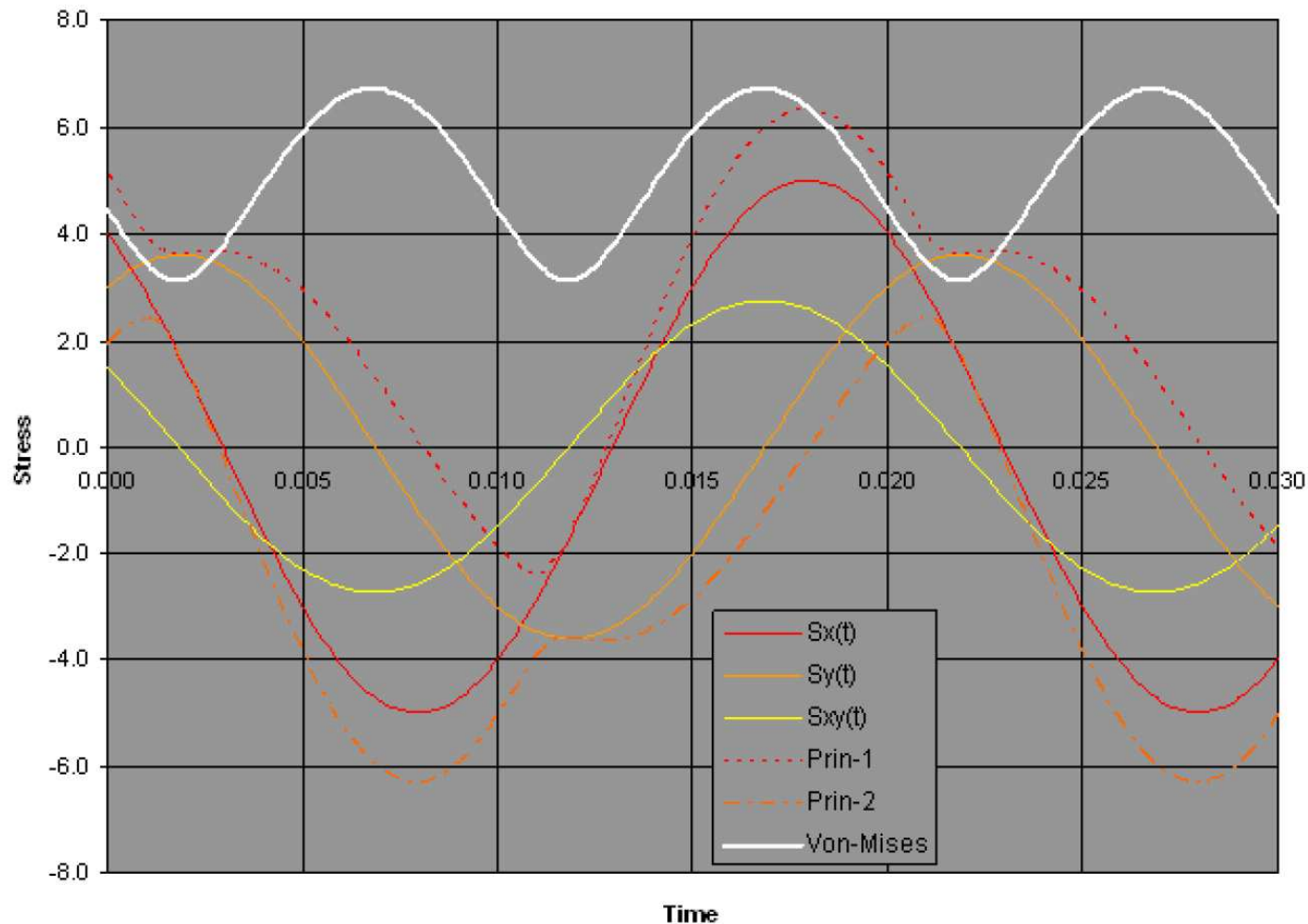


Figure from: MSC.Patran Documentation - Basic Functions, Chapter 11, Random Analysis

- Probability distribution of von Mises stress is neither Gaussian nor centered about zero
- Therefore, the RMS of basic stress tensor cannot be used
- The von Mises formula is correct only in its complex version and phase information is needed
- In a random analysis there is no phase information and so the correct von Mises can't be calculated
- Pitoiset e.a. [1] showed a method to derive von Mises PSD response, which is implemented in MSC.Random based on the deterministic frequency response
- MSC.Random is part of MSC.Patran

[1] X. Pitoiset, A. Preumont, A. Kernilis: Tools for a Multiaxial Fatigue Analysis of Structures Submitted to Random Vibrations. ESA SP-428, February 1999

➤ The formula given in [1] to derive von Mises PSD reads:

$$G_{\sigma_{vM}}(f_m) = \text{trace} \{ [A] [G_{\sigma\sigma}(f_m)] \}$$

with:

$$G_{\sigma\sigma}(f_m) = \bar{S} S^T$$

and the complex stress components

$$S^T = \begin{bmatrix} H_{s_x} & H_{s_y} & H_{s_z} & H_{s_{xy}} & H_{s_{xz}} & H_{s_{yz}} \end{bmatrix}$$

$\bar{S}$  contains the conjugate complex values of the stress components

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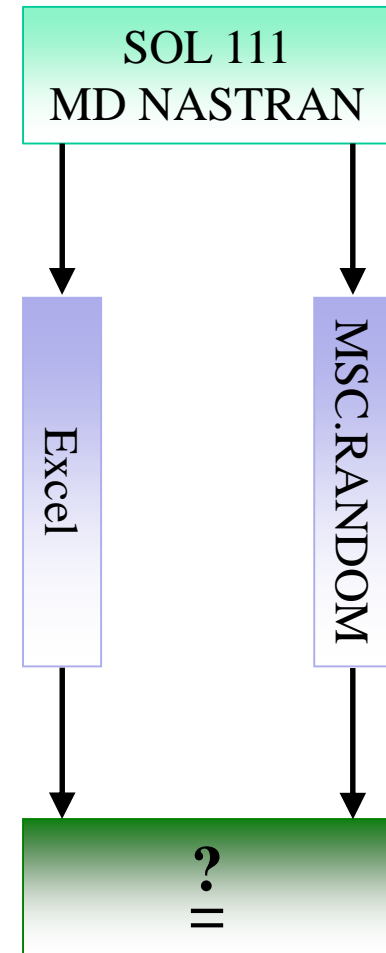
➤ Matrix [A] is derived from the quadratic formulation of von Mises stress and for the 3-dimensional case reads:

$$[A] = \begin{bmatrix} 1 & -0.5 & -0.5 & & & \\ -0.5 & 1 & -0.5 & & & \\ -0.5 & -0.5 & 1 & & & \\ & & & 3 & & \\ & & & & 3 & \\ & & & & & 3 \end{bmatrix}$$

and so for the 2-dimensional case reads:

$$[A] = \begin{bmatrix} 1 & -0.5 & \\ -0.5 & 1 & \\ & & 3 \end{bmatrix}$$

- The PSD von Mises stress is verified using a model of a flat plate (One solid and one shell model)
- Input to the formula are deterministic frequency response results from Nastran
- Results of MSC.Random are compared with those derived in Excel using above mentioned formula





➤ Two solid elements with high and low stresses are chosen

Element 41

| Elm 41 |    |           |           |           |           |           |           | Theory      | MSC.Random  |
|--------|----|-----------|-----------|-----------|-----------|-----------|-----------|-------------|-------------|
| Hz     |    | S_x       | S_y       | S_z       | S_xy      | S_xz      | S_yz      | v_Mises     | v_Mises     |
| 30     | Re | 2.44E-01  | 6.38E-02  | 3.93E-02  | 1.84E-02  | 3.25E-03  | 9.75E-04  | 3.87268E-02 | 3.87268E-02 |
|        | Im | -3.16E-03 | -8.11E-04 | -4.93E-04 | -2.56E-04 | -4.28E-05 | -2.84E-05 |             |             |
| 40     | Re | 2.54E-01  | 6.62E-02  | 4.07E-02  | 1.92E-02  | 3.37E-03  | 1.06E-03  | 4.17892E-02 | 4.17892E-02 |
|        | Im | -4.57E-03 | -1.17E-03 | -7.12E-04 | -3.70E-04 | -6.19E-05 | -4.12E-05 |             |             |
| 50     | Re | 2.67E-01  | 6.96E-02  | 4.28E-02  | 2.03E-02  | 3.55E-03  | 1.19E-03  | 4.63120E-02 | 4.63120E-02 |
|        | Im | -6.38E-03 | -1.64E-03 | -9.93E-04 | -5.17E-04 | -8.64E-05 | -5.78E-05 |             |             |

Element 50

| Elm 50 |    |           |           |           |           |           |           | Theory      | MSC.Random  |
|--------|----|-----------|-----------|-----------|-----------|-----------|-----------|-------------|-------------|
| Hz     |    | S_x       | S_y       | S_z       | S_xy      | S_xz      | S_yz      | v_Mises     | v_Mises     |
| 30     | Re | 1.32E-03  | -2.04E-03 | -6.17E-05 | -1.15E-03 | -1.13E-04 | -2.39E-04 | 1.27154E-05 | 1.27155E-05 |
|        | Im | -2.60E-05 | 3.47E-05  | 1.51E-06  | 1.93E-05  | 1.90E-06  | 4.52E-06  |             |             |
| 40     | Re | 1.40E-03  | -2.15E-03 | -6.66E-05 | -1.21E-03 | -1.18E-04 | -2.54E-04 | 1.41516E-05 | 1.41516E-05 |
|        | Im | -3.78E-05 | 5.04E-05  | 2.21E-06  | 2.80E-05  | 2.76E-06  | 6.57E-06  |             |             |
| 50     | Re | 1.52E-03  | -2.30E-03 | -7.35E-05 | -1.29E-03 | -1.27E-04 | -2.74E-04 | 1.63131E-05 | 1.63131E-05 |
|        | Im | -5.31E-05 | 7.07E-05  | 3.11E-06  | 3.92E-05  | 3.87E-06  | 9.23E-06  |             |             |

- Two shell elements with high and low stresses are chosen

Element 10

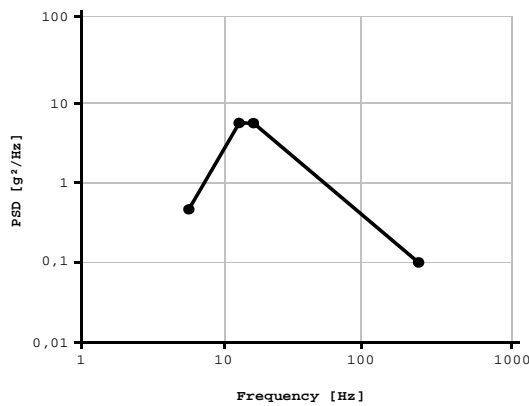
| Elm 10 | S <sub>x</sub> |          | S <sub>y</sub> |           | S <sub>xy</sub> |           | Theory      |  | MSC.Random  |  |
|--------|----------------|----------|----------------|-----------|-----------------|-----------|-------------|--|-------------|--|
|        | Re             | Im       | Re             | Im        | Re              | Im        | v_Mises     |  | v_Mises     |  |
| 30     | -2.64E-03      | 5.25E-05 | 3.90E-03       | -6.70E-05 | 2.22E-03        | -3.77E-05 | 4.73121E-05 |  | 4.73121E-05 |  |
| 40     | -2.81E-03      | 7.65E-05 | 4.11E-03       | -9.74E-05 | 2.34E-03        | -5.49E-05 | 5.27718E-05 |  | 5.27718E-05 |  |
| 50     | -3.05E-03      | 1.08E-04 | 4.41E-03       | -1.37E-04 | 2.50E-03        | -7.71E-05 | 6.10231E-05 |  | 6.10231E-05 |  |

Element 11

| Elm 10 | S <sub>x</sub> |          | S <sub>y</sub> |          | S <sub>xy</sub> |          | Theory      |  | MSC.Random  |  |
|--------|----------------|----------|----------------|----------|-----------------|----------|-------------|--|-------------|--|
|        | Re             | Im       | Re             | Im       | Re              | Im       | v_Mises     |  | v_Mises     |  |
| 30     | -5.51E-01      | 7.30E-03 | -1.57E-01      | 2.07E-03 | -5.20E-03       | 7.88E-05 | 2.42096E-01 |  | 2.42096E-01 |  |
| 40     | -5.73E-01      | 1.06E-02 | -1.63E-01      | 2.99E-03 | -5.44E-03       | 1.14E-04 | 2.61690E-01 |  | 2.61690E-01 |  |
| 50     | -6.04E-01      | 1.48E-02 | -1.72E-01      | 4.19E-03 | -5.78E-03       | 1.60E-04 | 2.90820E-01 |  | 2.90820E-01 |  |

- The results of MSC.Random compare very well with those derived manually

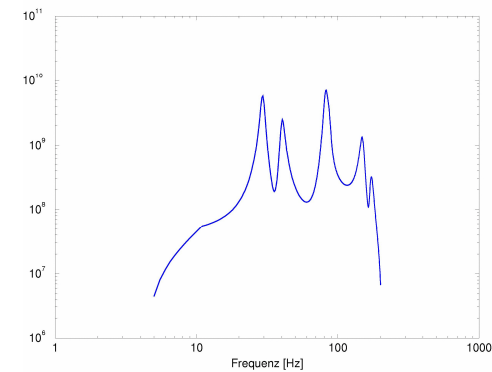
- A standard frequency response analysis with unity load is done using MD Nastran
- The results are attached to MSC.Random
- Load PSD is put in to MSC.Random
- Random response results are derived in MSC.Random



LOAD PSD

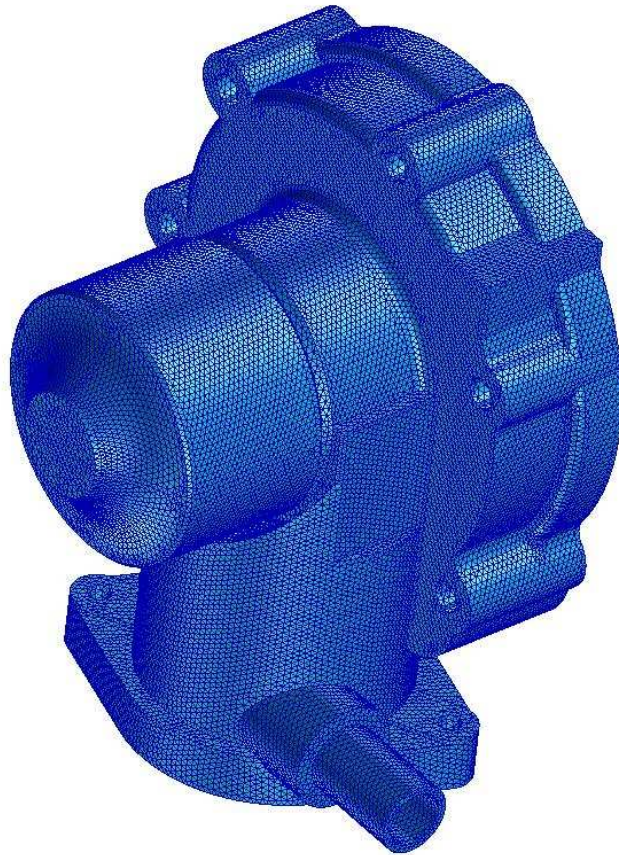
SOL 111  
MD NASTRAN

MSC.RANDOM

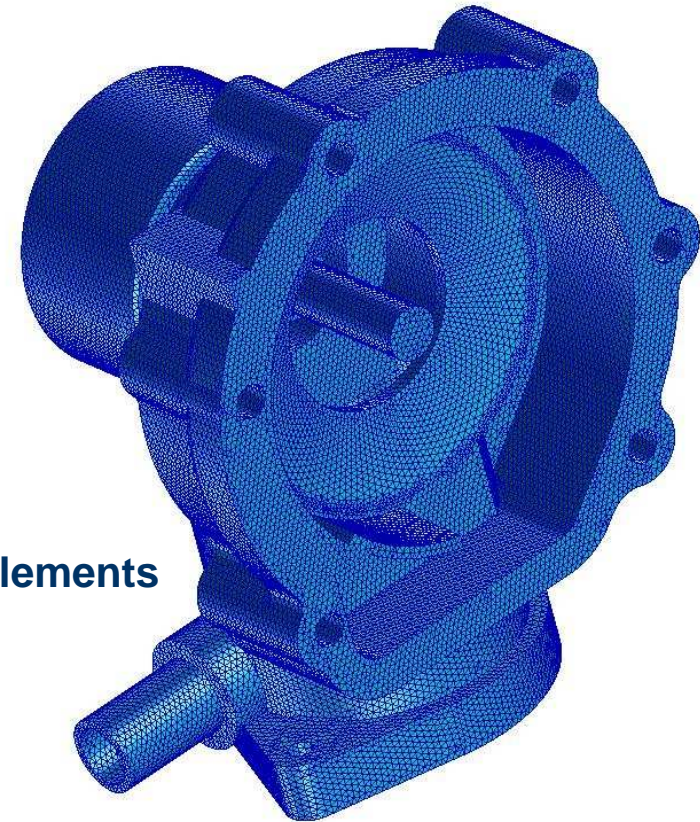


RESULT PSD

➤ Cooling Water Pump for car – FE Model



**911 882 Nodes**  
**582 879 Tet10-Elements**



➤ Shaker test with random excitation

Performance Data (911 882 nodes, 582 879 Tet10, displacement and stress)

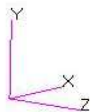
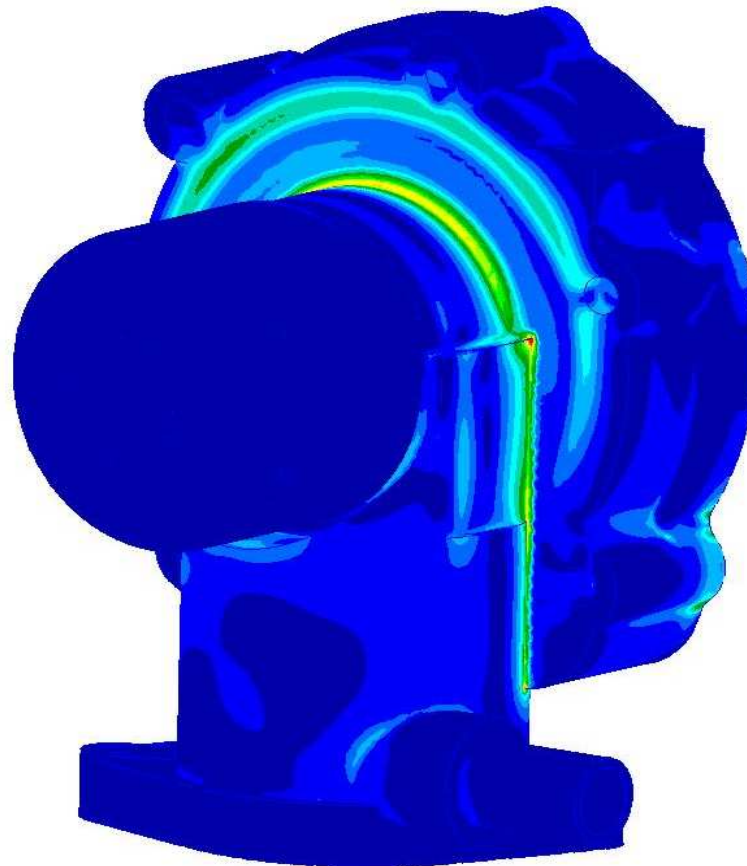
- Nastran Frequency Response:
  - 27h 22min (elapsed), 14h 56min (CPU), 206GB disk space
  - Results: xdb file of 57.5GB
  
- Creating RMS Results using MSC.Random:
  - 2h 19min – run in background via Patran batch mode
  
- Plotting RMS Results and generating PSD plots takes only seconds
  
- All data derived on AMD Opteron under Windows 64bit



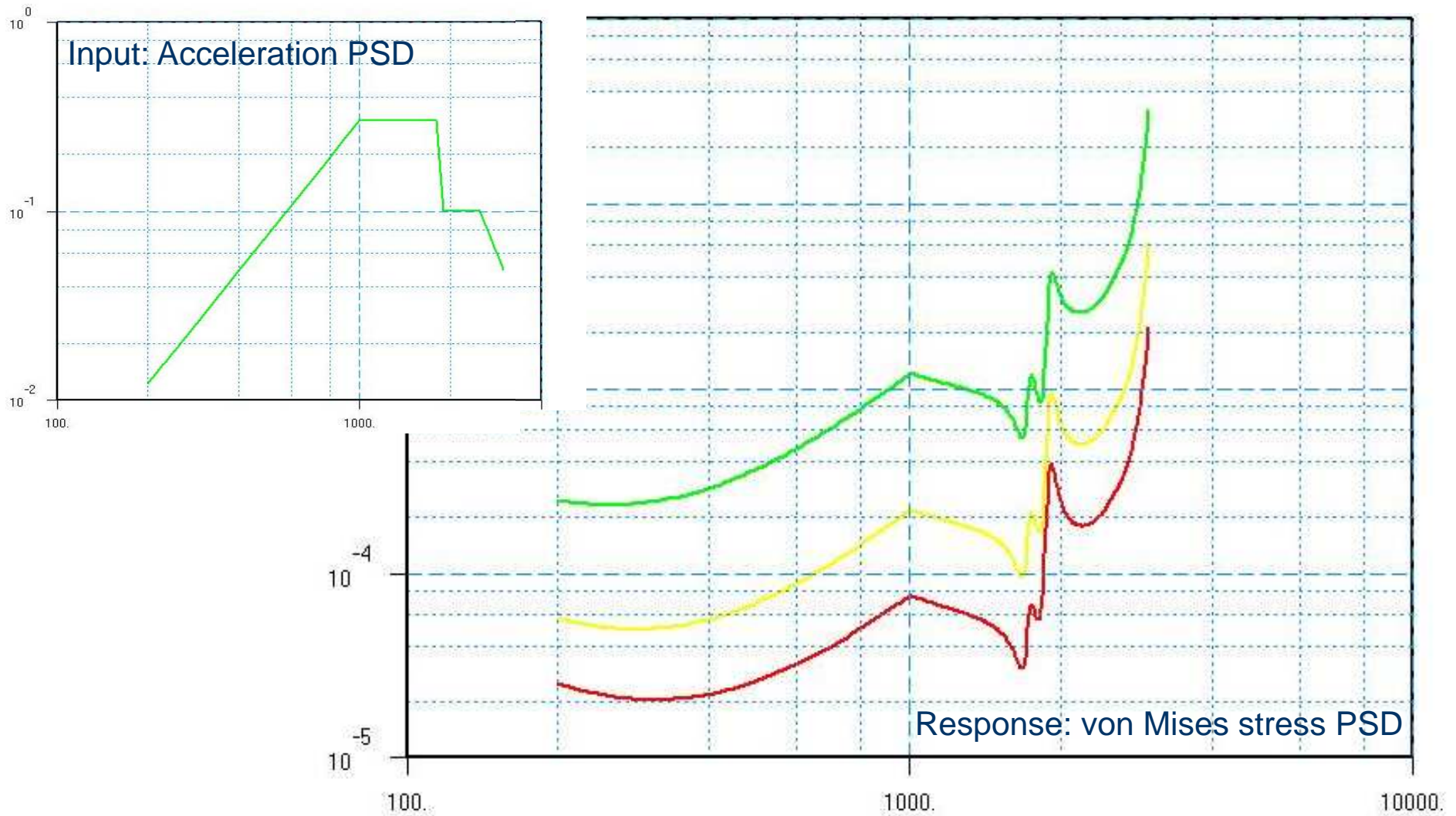
➤ RMS-Data for "Hot Spot" identification delivers a fast overview of critical areas

Patran 2010.2.2 64-Bit (MD Enabled) 13-May-11 10:11:12

Fringe: RMS, Random, Stress Solids, Von-Mises, , At Non-Layered



➤ PSD-Data for finding responsible resonances



- Often von Mises stresses are requested in dynamic analysis
- Phase information needed is only available in a frequency response simulation
- Von Mises cannot be computed correctly out of a random analysis because the phase is missing
- *But most postprocessors offer this option!*
- The only way to calculate the von Mises stress PSD is based on the deterministic frequency response
- A correct and fast way to get valid von Mises stresses is to use MSC.Random



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