

DAMPING VALUES IN AEROSPACE STRUCTURES AND COMPONENTS  
Revision D

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| Table 1. Typical Q values for Structures and Components                  |            |               |         |          |
|--|------------|---------------|---------|----------|
| System   | fn (Hz)    | Damping Ratio | Q       | Appendix |
| Pegasus XL Launch Vehicle Body-Bending during Drop Transient             | 9.9        | 1.0%          | 50      | A        |
| Fairing Ring Frequency   | 897        | 3.7%          | 13.5    | B        |
| Battery Cells inside Foam-lined Box                                      | 80         | 15.2%         | 3.3     | C        |
| Avionics Circuit Boards, Hardmounted Boxes                               | 220 to 650 | 1.7% to 5.6%  | 9 to 29 | D        |
| Component Mounting Brackets  | 70 to 2000 | 2% to 50%     | 1 to 25 | E        |
| Avionics Boxes Mounted via Lord Isolators                                | 27 to 31   | 8.3%          | 6       | F        |
| Flexible Confined Detonating Cord (FCDC)                                 | 8 to 107   | 6%            | 8.3     | G        |
| Space Integrated GPS/INS (SIGI) Inertial Sensor Assembly (ISA) Isolators | 55         | 13.5%         | 3.7     | H        |

| Table 1. Typical Q values for Structures and Components (continued) |         |               |     |          |
|---|---------|---------------|-----|----------|
| System  | fn (Hz) | Damping Ratio | Q   | Appendix |
| Circular Bulkhead, Homogeneous                                      | 57      | 6.5%          | 7.7 | I        |
| Circular Bulkhead, Honeycomb Sandwich                               | 40      | 5.9%          | 8.5 | J        |

Excerpt from NASA SP-8050, Structural Vibration Prediction.

| Type of Structure  | Percent of Critical Viscous Damping | Remarks   |
|--|-------------------------------------|---|
| Homogeneous-element configurations (machined brackets, solid beams, welded construction) | 1 to 2                              | Damping factor depends on stress levels induced during vibration  |
| Riveted or bolted structures   | 3 to 10                             | Damping cause by friction at joints significantly reduces the vibration amplification                   |
| Laminated plastics   | 4 to 10                             | Phenolic laminate   |
| Honeycomb-core panels  | 3 to 6                              | Damping factor depends on method of fabrication (brazed versus adhesive bond) and on acoustic radiation |
| Vibration-isolated components  | 10 to 20                            | Damping factor depends on the isolator design   |
| Nonviscous fluids  | 0.5                                 | Frequency < 5 Hz  |
|  | 1.0                                 | 5 Hz ≤ Frequency ≤ 15 Hz  |
|  | 1.5                                 | Frequency > 15 Hz   |

Excerpt from NASA SP-8079, Structural Interaction with Control Systems

| Vehicle         | Vibration Mode | Frequency (Hz) | Damping Ratio |
|-----------------|----------------|----------------|---------------|
| Saturn V/Apollo | First          | 1.0            | 0.005         |
|                 | Second         | 1.7            | 0.007         |
|                 | Third          | 2.3            | 0.006         |
|                 | Fourth         | 3.0            | 0.010         |

The damping values were measured during a modal test.

APPENDIX A

Pegasus Launch Vehicle Body-Bending during Drop Transient

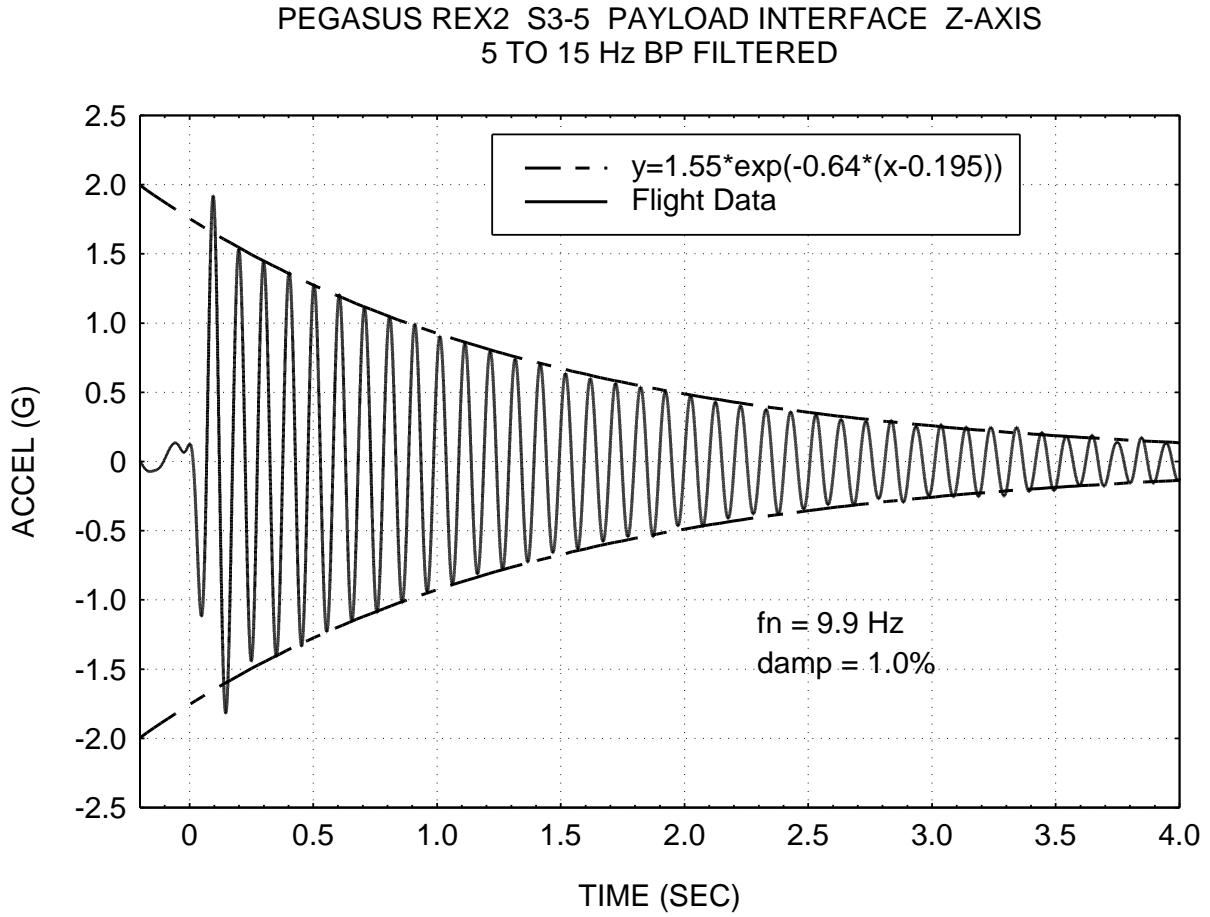


Figure A-1.

## APPENDIX B

### Fairing Ring Frequency

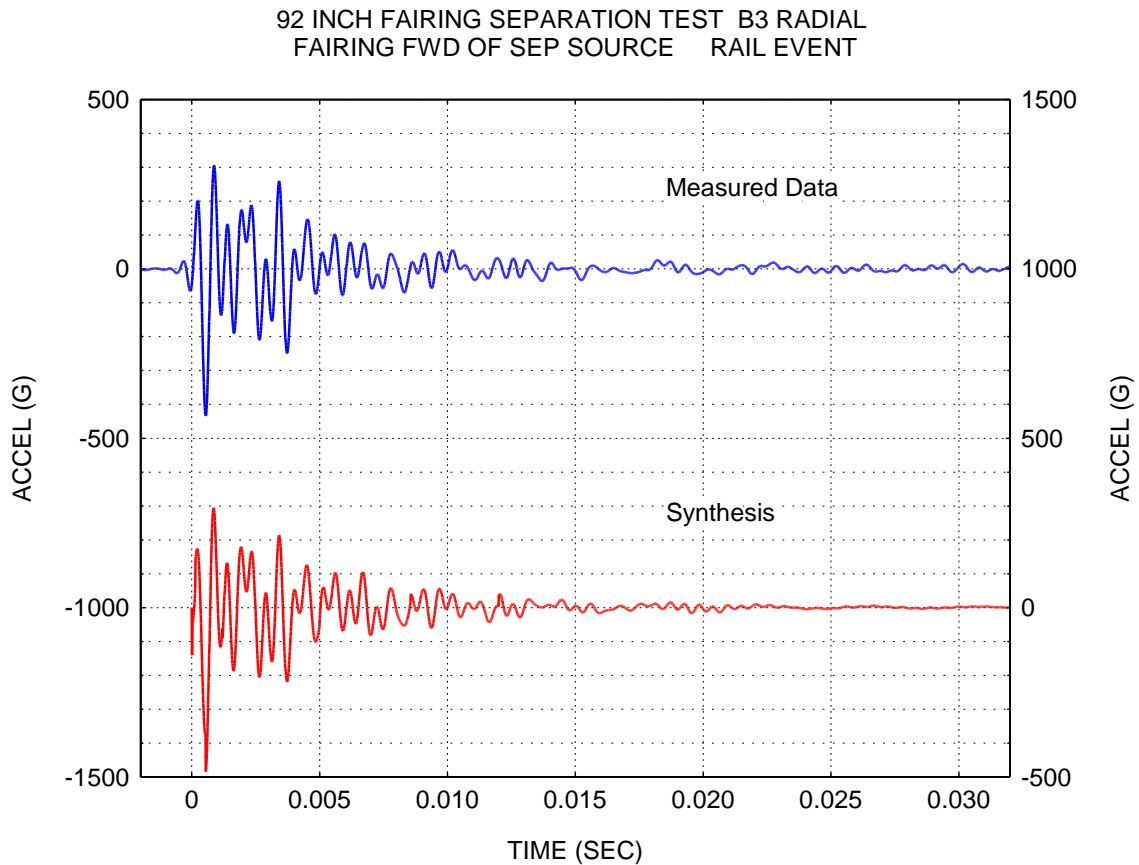


Figure B-1.

The source device was a frangible joint rail. The data was measured during a ground test.

The fairing consists of graphite-epoxy skins over an aluminum honeycomb core.

Note that the data is bandpass filtered from 20 to 2000 Hz.

The fairing's ring frequency is

$$f_n = \frac{C_L}{\pi d} \quad (\text{B-1})$$

|       |   |                |  |
|-------|---|----------------|--|
| $C_L$ | = | 257,976 in/sec | Longitudinal wave speed in the composite skin material |
| $d$   | = | 92 in          | Diameter   |

$$f_n = \frac{257,976 \text{ in/sec}}{\pi(92 \text{ in})} = 893 \text{ Hz}$$

The synthesis consists of ten components. The first three are given in Table 2.

| Table B-1. Synthesis Results |         |           |             |         |             |
|------------------------------|---------|-----------|-------------|---------|-------------|
| N                            | Amp (G) | Freq (Hz) | Phase (rad) | Damping | Delay (sec) |
| 1                            | 186.2   | 1888.895  | 1.682       | 0.017   | 0.000       |
| 2                            | 172.7   | 897.063   | 3.609       | 0.037   | 0.000       |
| 3                            | 112.6   | 1573.298  | 1.648       | 0.026   | 0.001       |

The second component represents the ring frequency.

APPENDIX C

Battery Cells inside Foam-lined Box

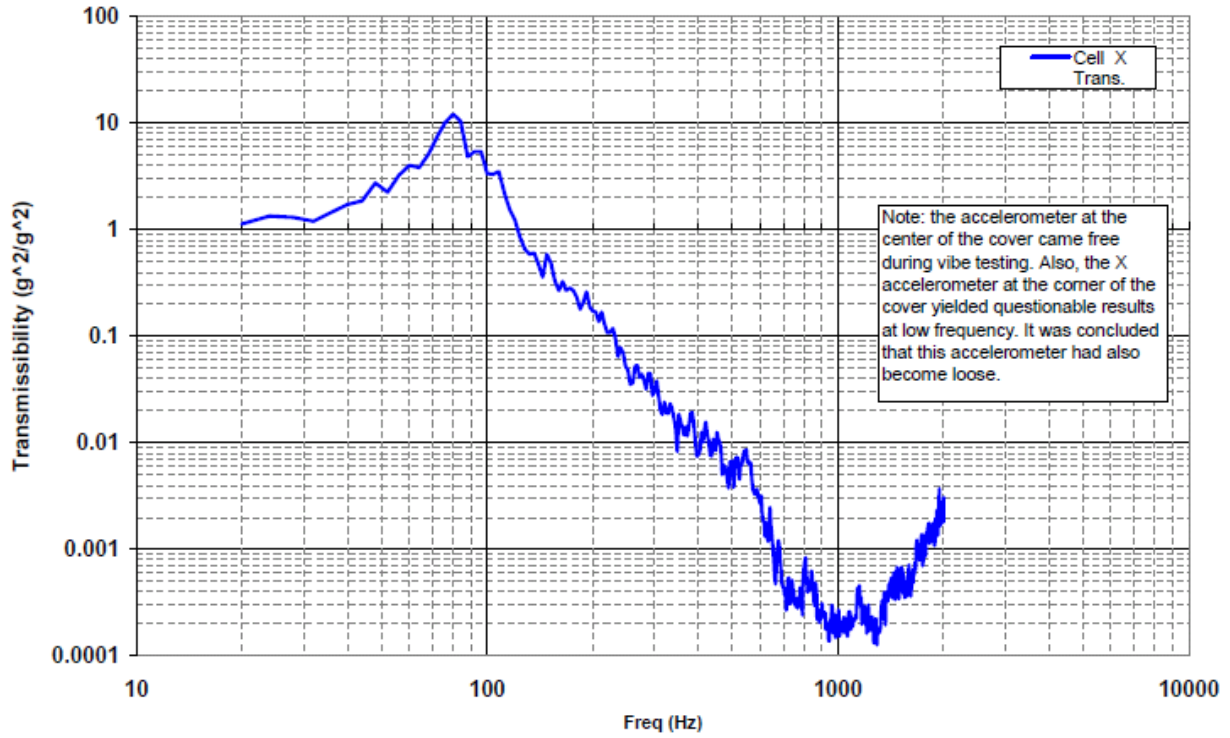
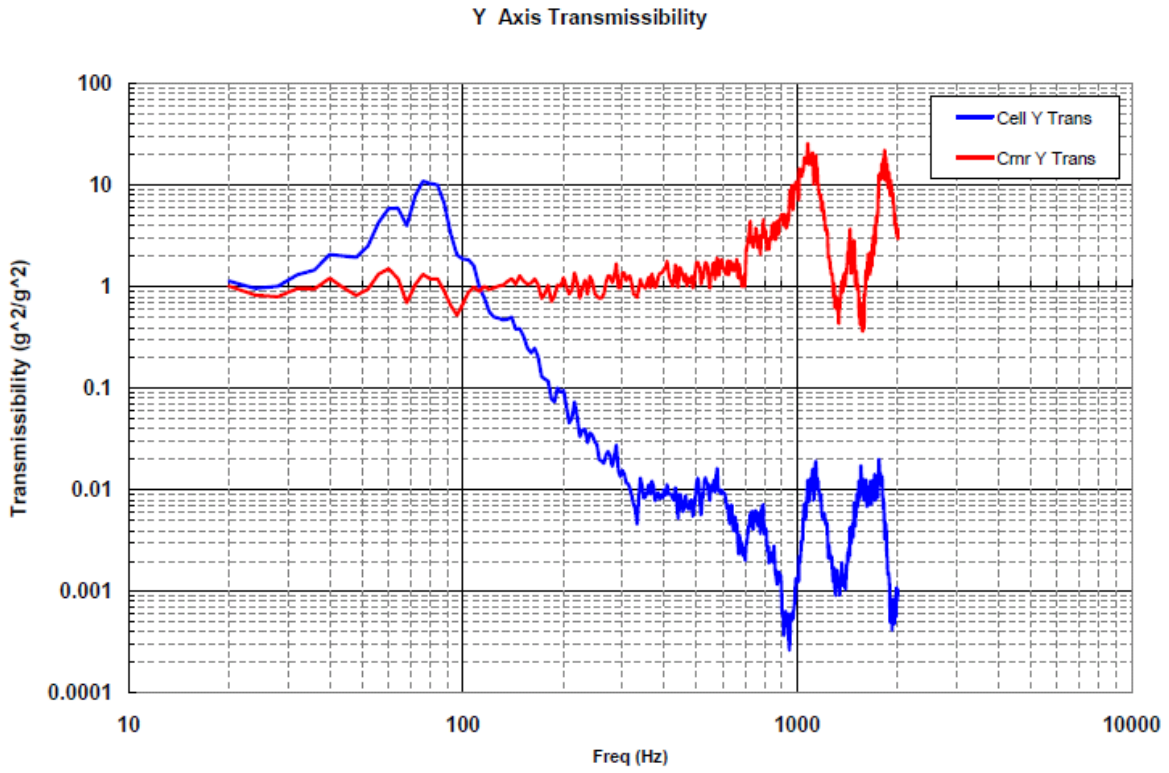


Figure 19: X Axis Transmissibility to Cells

Figure C-1.

The X-axis is vertical.

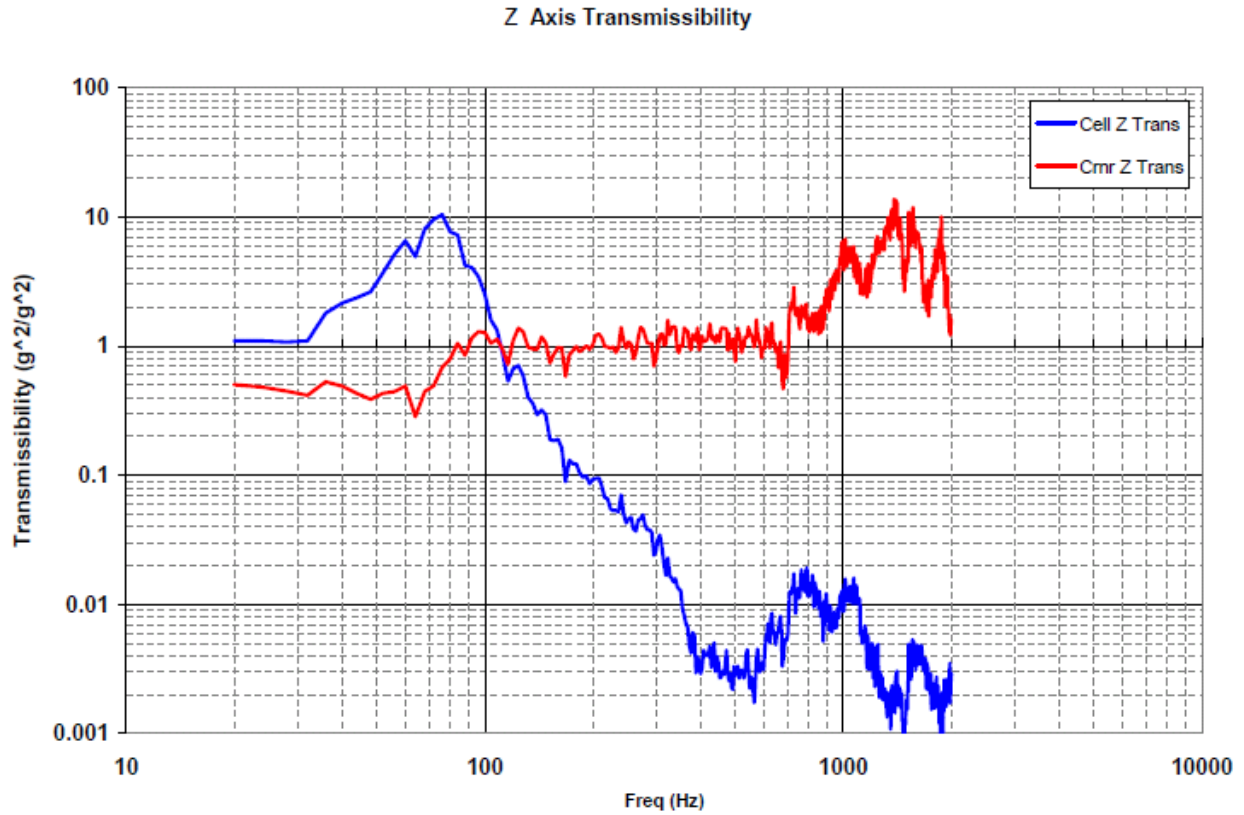


**Figure 23: Y Axis Transmissibilities**

Figure C-2.

The Y-axis is a lateral axis.





**Figure 27: Z Axis Transmissibilities**

Figure C-3.

The Z-axis is a lateral axis.

Reference:

ME File:T042-040, Random and Sine Vibe Test, 2nd ACME Evaluation Battery, 2008.

## APPENDIX D

### Avionics Circuit Board

The 3 dB Bandwidth method is used to determine the Q value for the following avionics boxes.

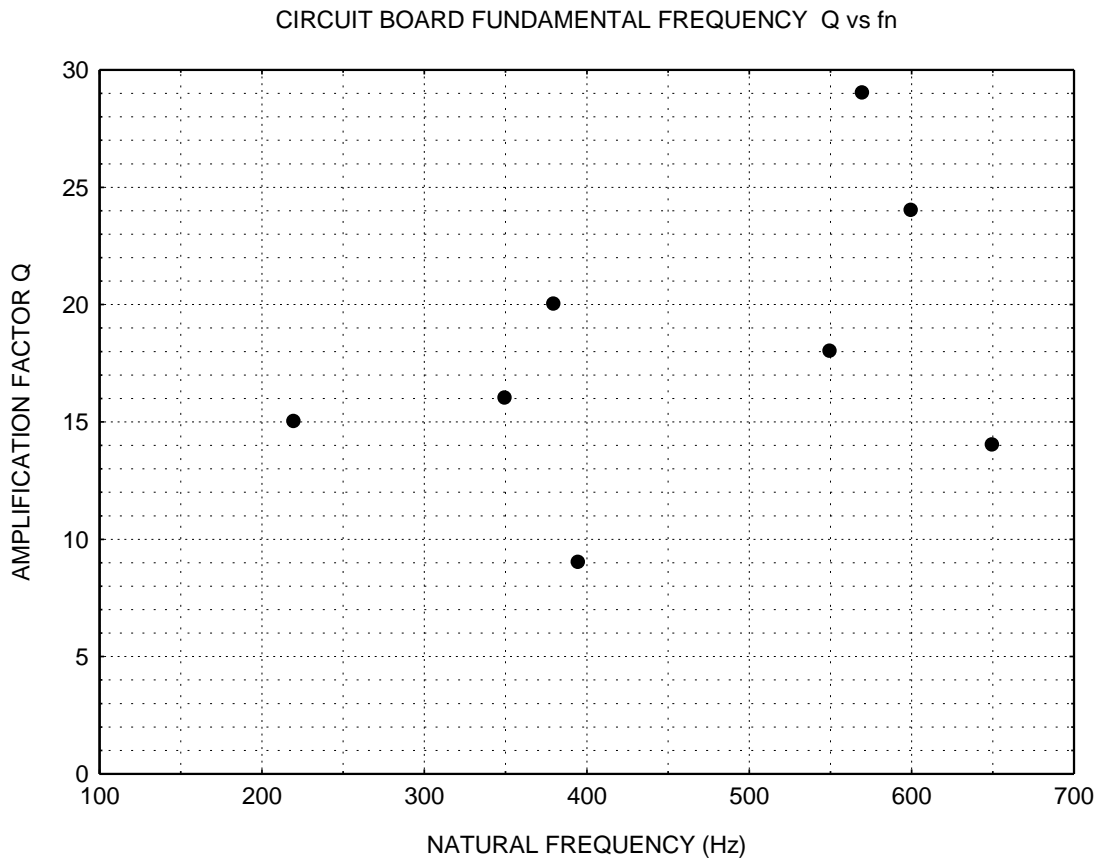


Figure D-1.

| Table D-1. Q at Fundamental Frequency |         |                      |    |
|---------------------------------------|---------|----------------------|----|
| n                                     | fn (Hz) | -3 dB Bandwidth (Hz) | Q  |
| 1                                     | 380     | 20                   | 19 |
| 2                                     | 220     | 15                   | 15 |
| 3                                     | 395     | 45                   | 9  |
| 4                                     | 550     | 30                   | 18 |
| 5                                     | 600     | 25                   | 24 |
| 6                                     | 570     | 20                   | 29 |
| 7                                     | 350     | 22                   | 16 |
| 8                                     | 650     | 45                   | 14 |

The range is 9 to 29. The average is 18.1 with a standard deviation of 6.2.

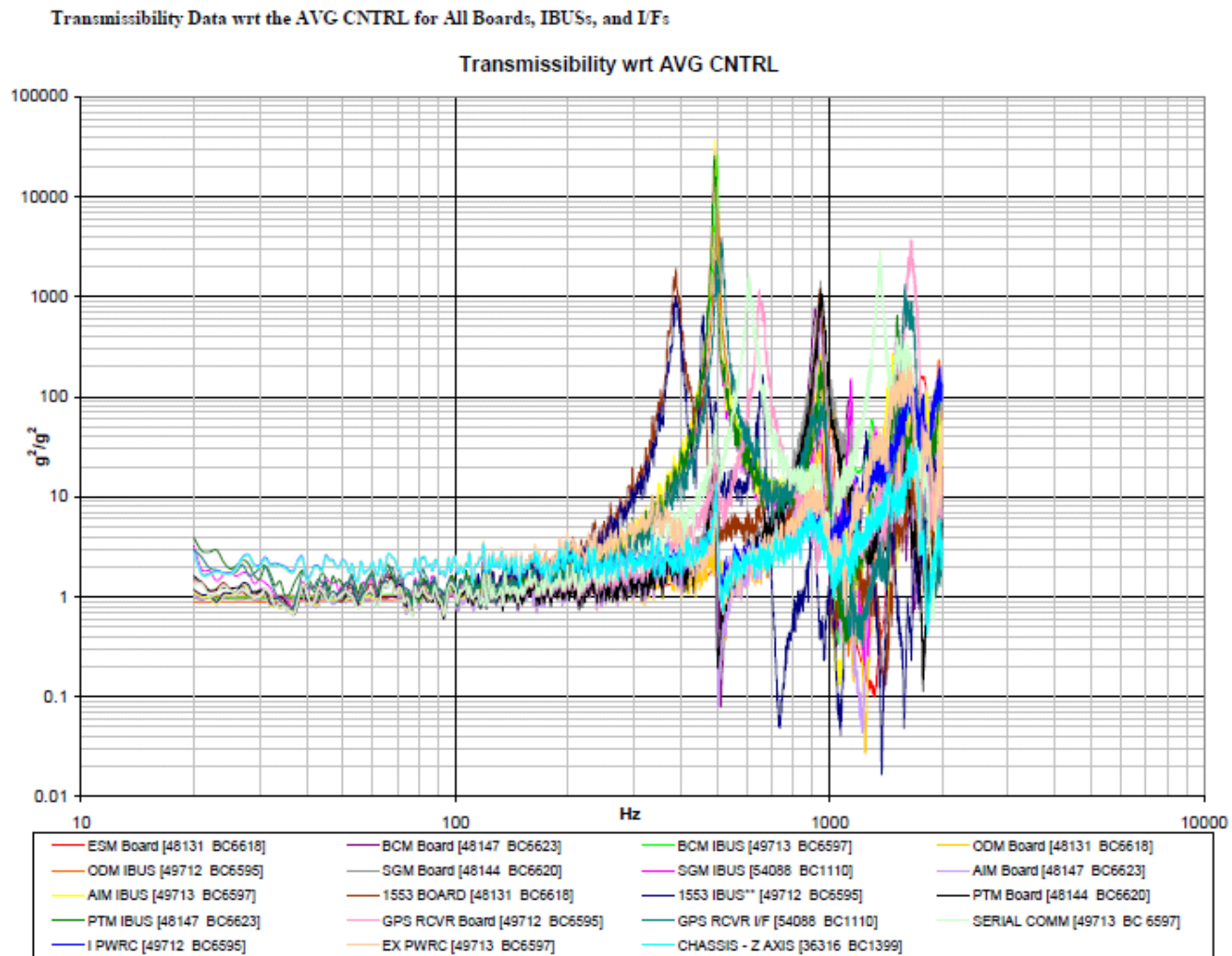


Figure D-1. Avionics Box 1

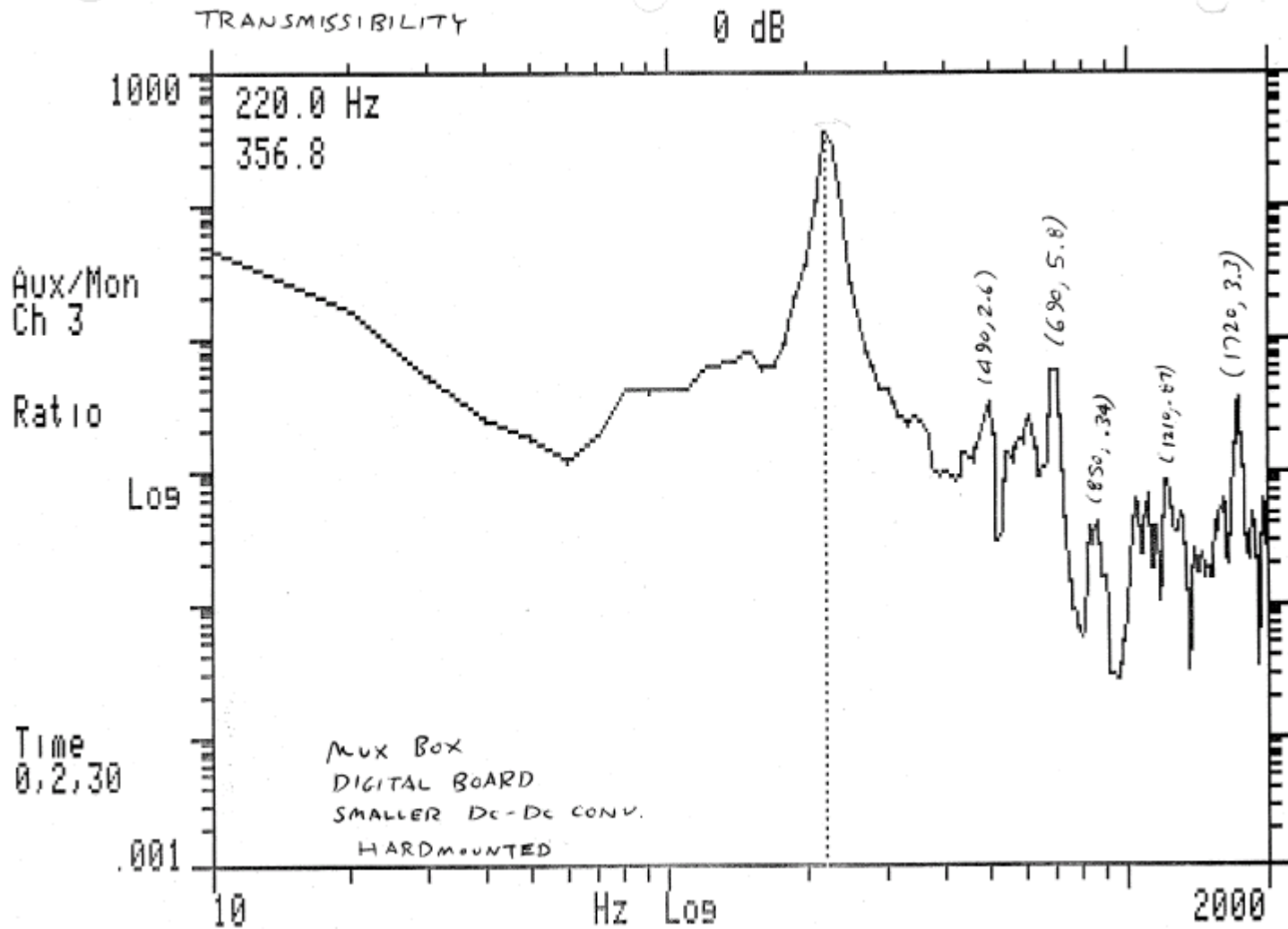


Figure D-2. Avionics Box 2

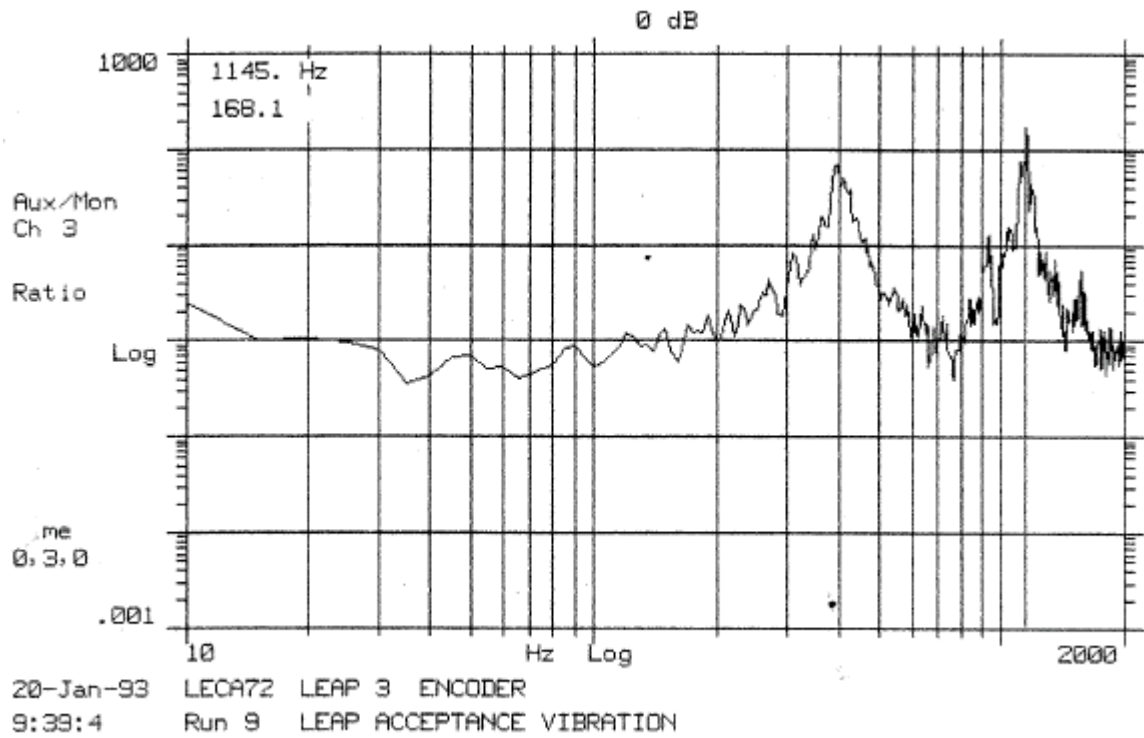


Figure D-3. Avionics Box 3

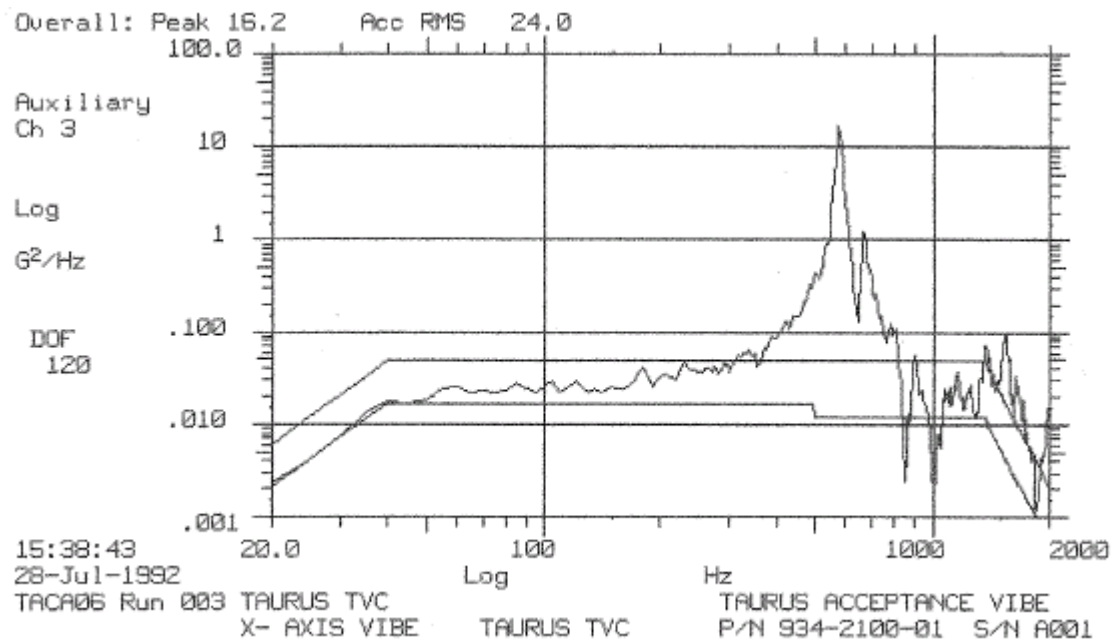


Figure D-4. Avionics Box 4

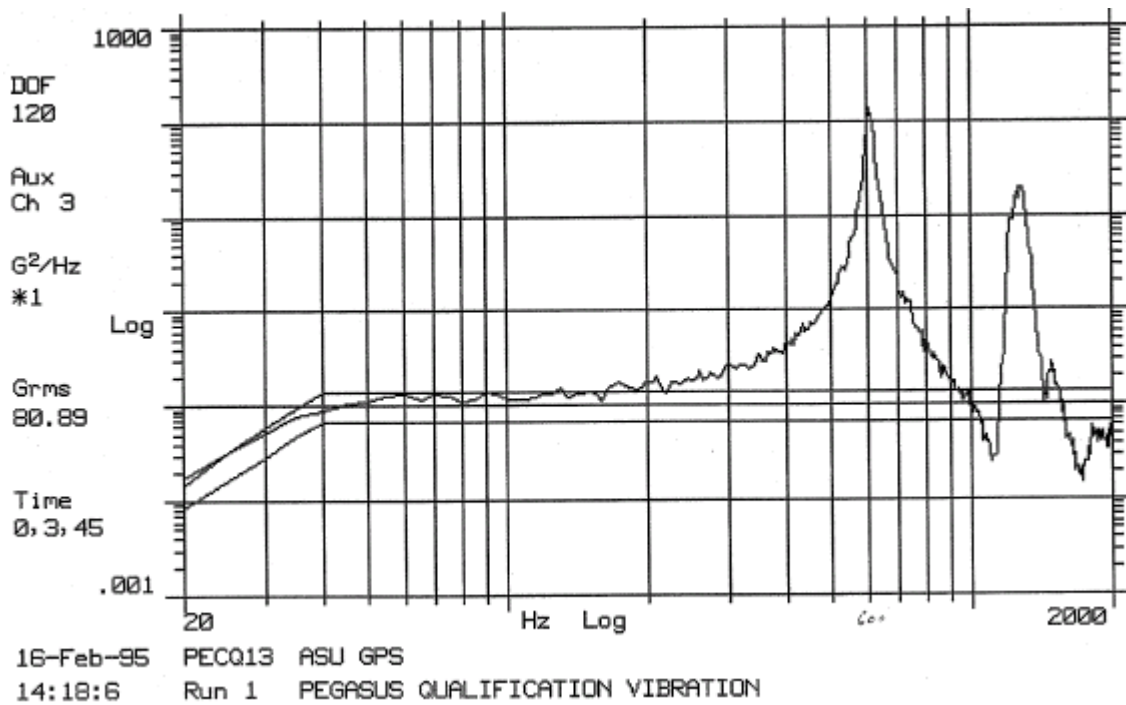


Figure D-5. Avionics Box 5

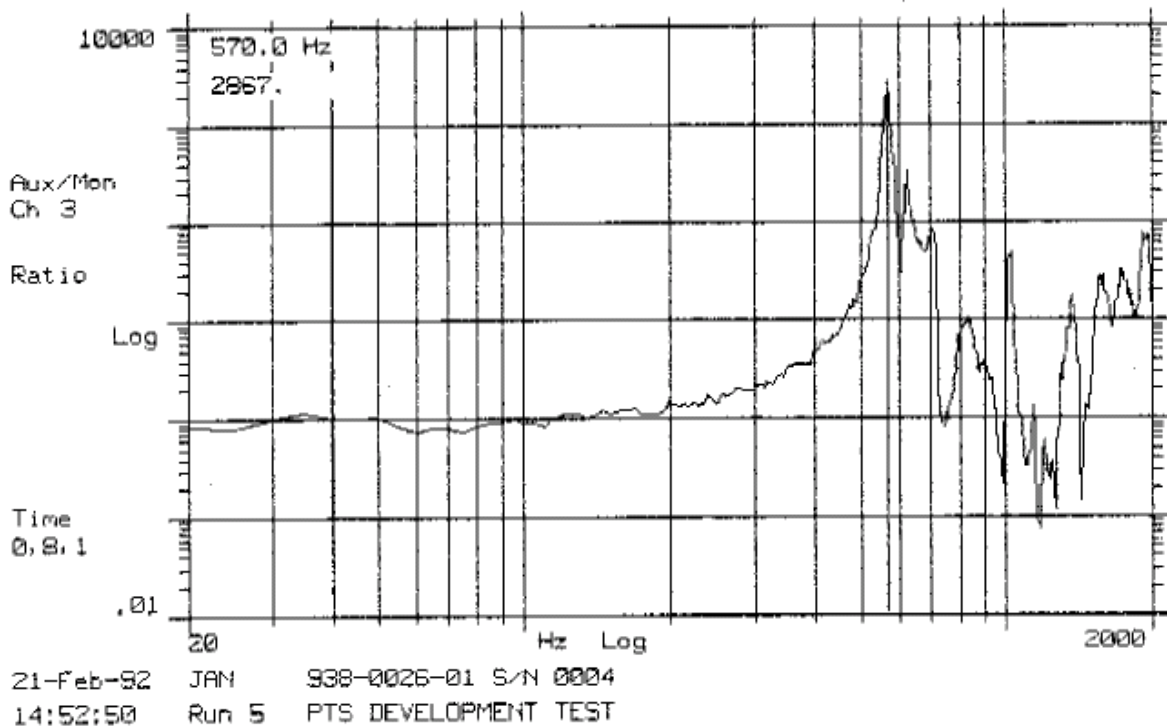
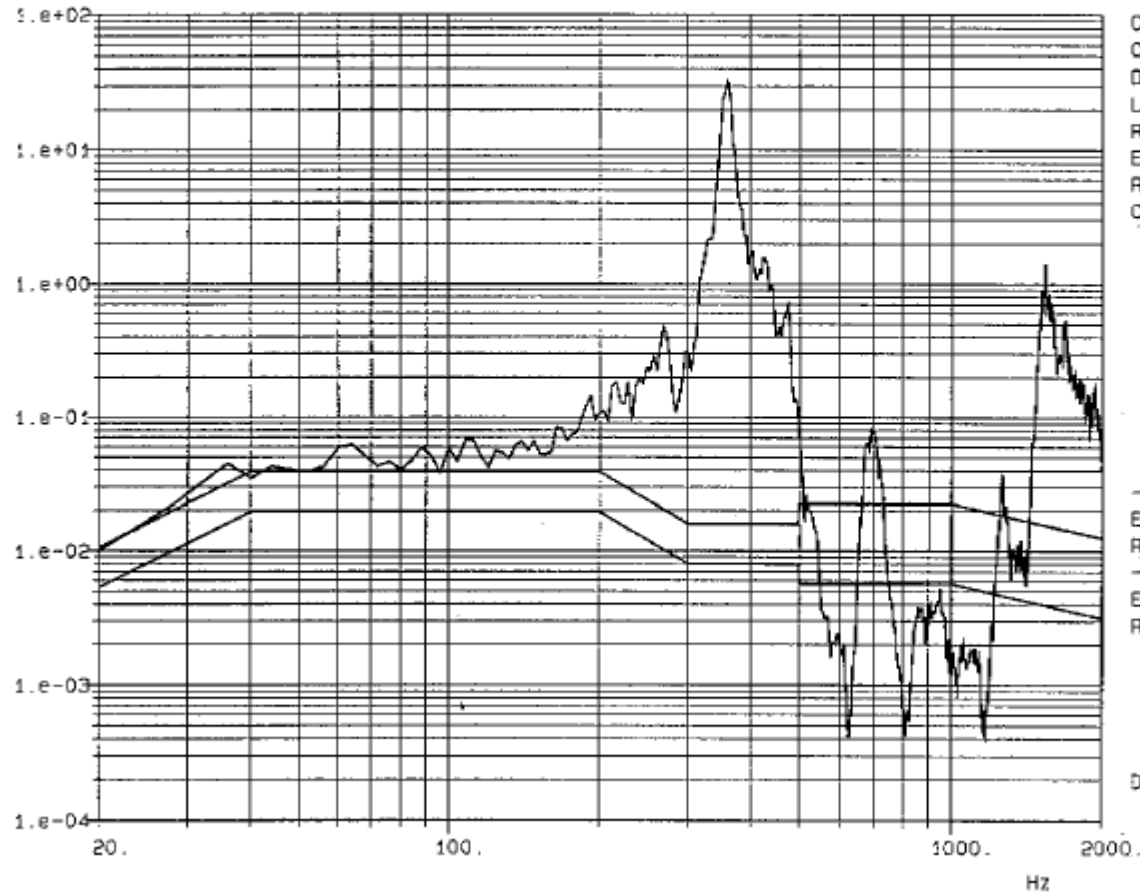


Figure D-6. Avionics Box 6

ait MACHBDX ACCEPT  
AIT MACH9 ENGEVAL Z 11JUL98 MACH9 ENG EVAL DR#20483 PII STP 005 Z AXIS

g<sup>2</sup>/Hz b/c 06660 on board ic mounted z axis



Chan. No. : 3  
Chan. Type : M  
DOF : 40  
Level : -6. dB  
Resolution : 4. Hz  
Eng. Unit : g  
RMS (act.) : 31.8973 g  
Contr. Mode: Closed loop

-- Time on act. level --  
Elapsed : 0:01:00  
Remaining : 0:00:00  
--- Time total ---  
Elapsed : 0:01:40  
Remaining : 0:00:00

Date : 5/16/1996  
22:39:12

Figure D-7. Avionics Box 7



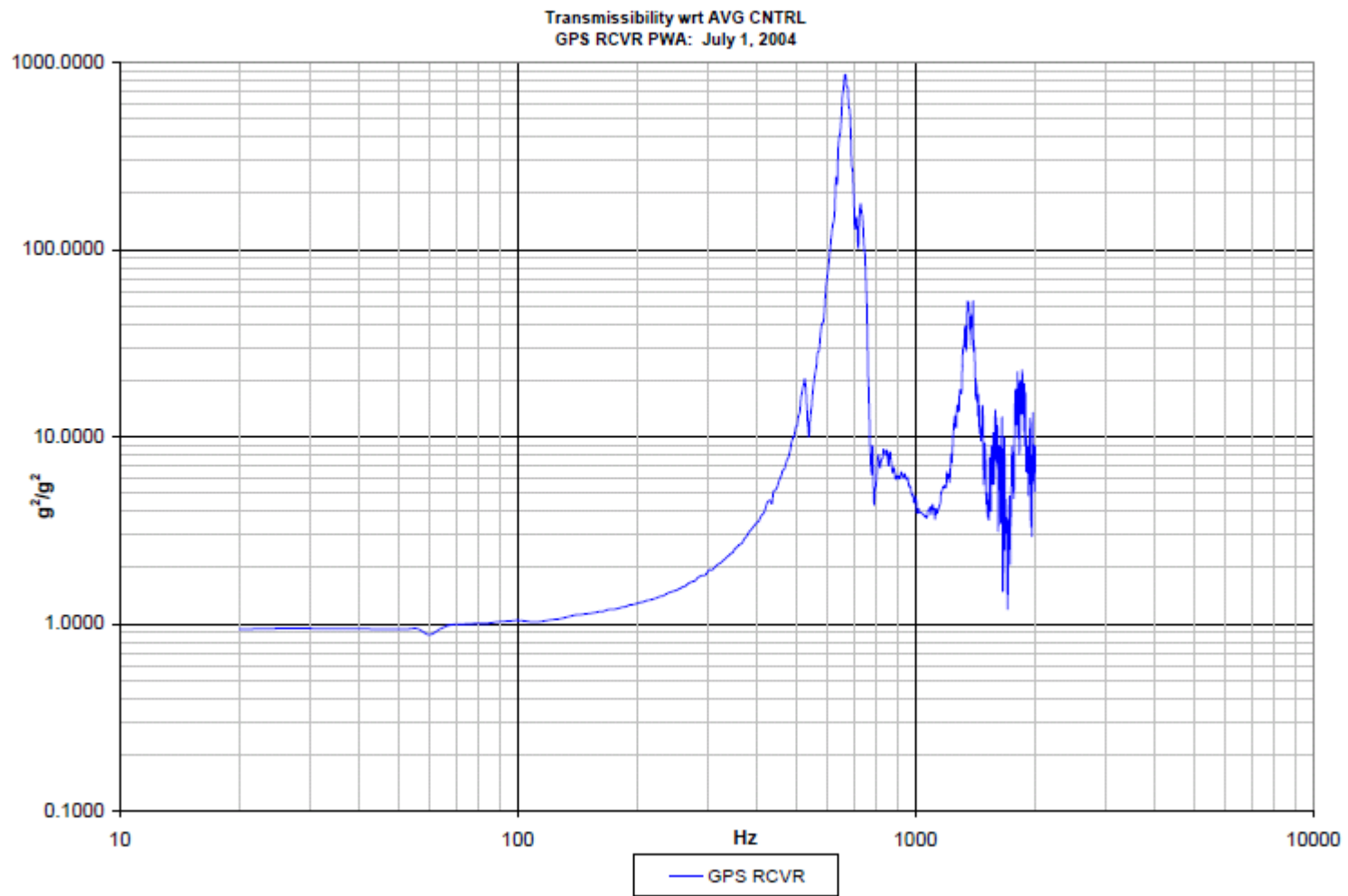


Figure D-8. Avionics Box 8

## APPENDIX E

### Component Mounting Brackets

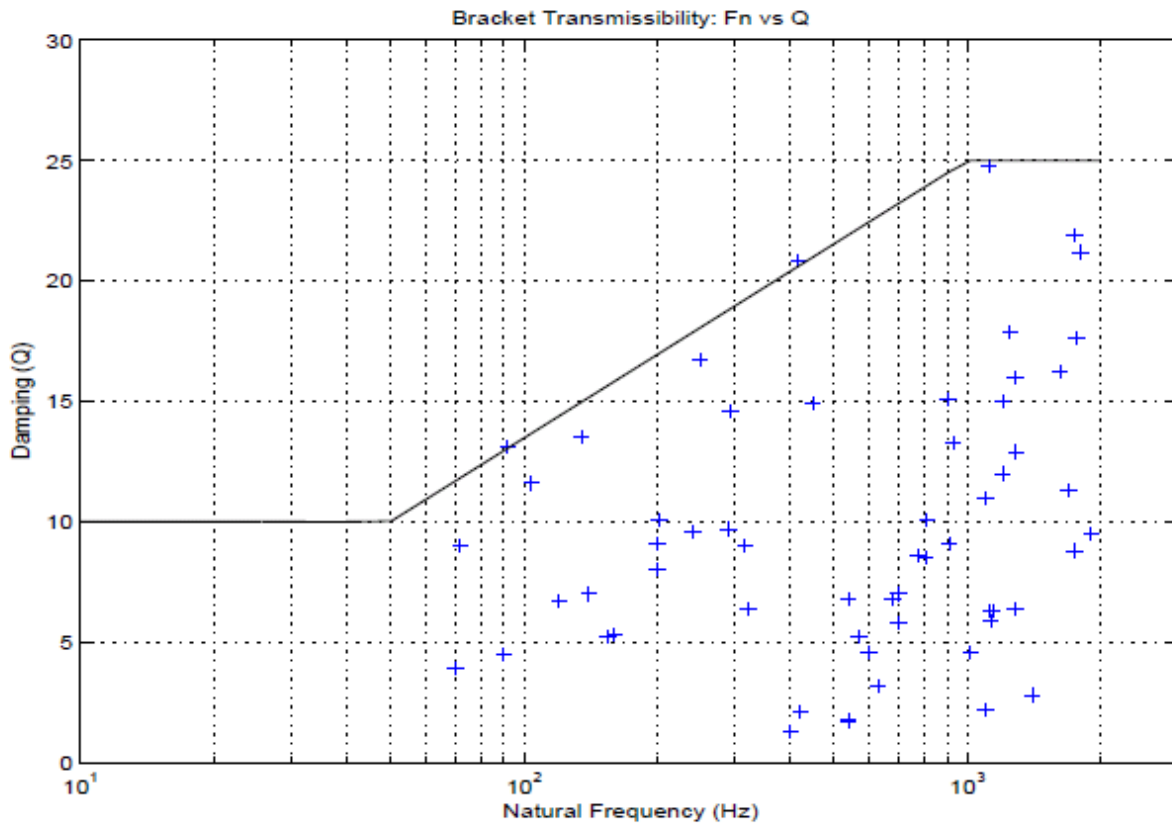


Figure 1: Bracket Mode Natural Frequency (Fn) vs. Damping (Q)

Equation 1:

|                                     |   |                                     |
|-------------------------------------|---|-------------------------------------|
| $Q = 10$                            | } | $fn \leq 100\text{Hz}$              |
| $Q = 11.53 * \log_{10}(fn) - 9.588$ |   | $100\text{Hz} < fn < 1000\text{Hz}$ |
| $Q = 25$                            |   | $fn \geq 1000\text{Hz}$             |

Figure E-1.

#### Reference

ME File: 030-356, Bracket Transmissibility Data Review, 2008.

## APPENDIX F

### Avionics Boxes Mounted via Lord Isolators

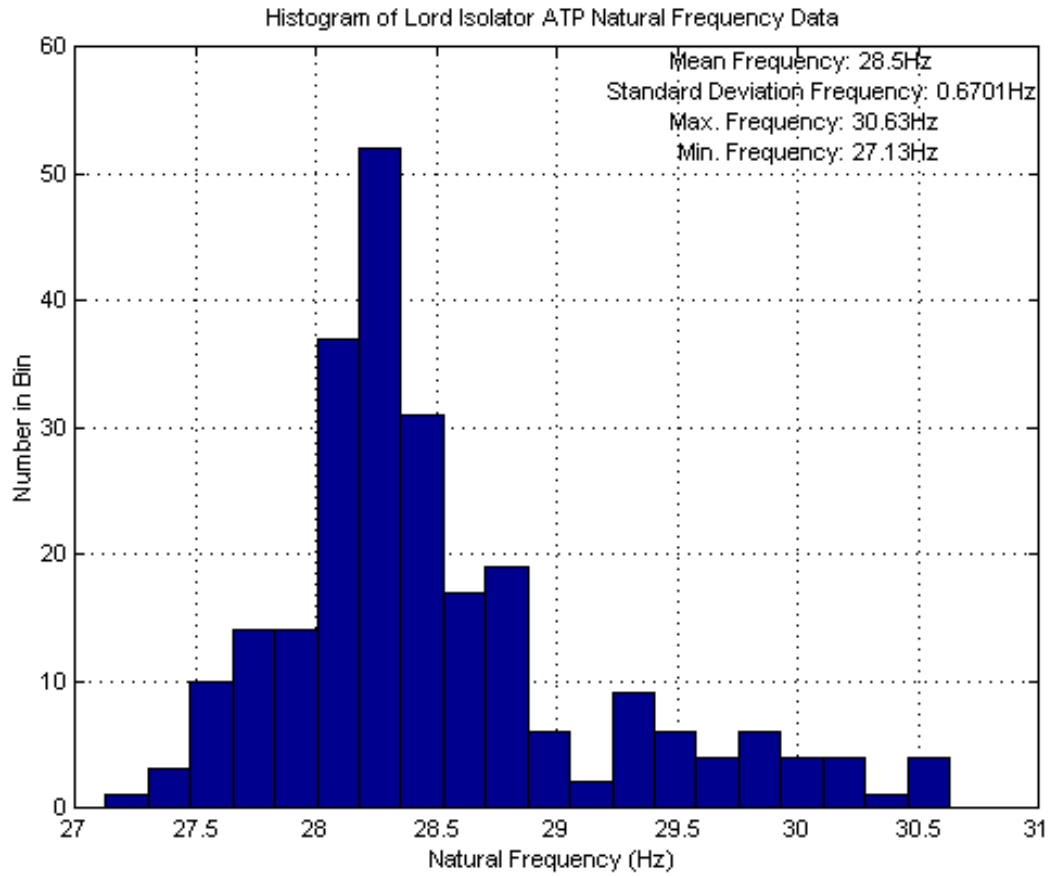


Figure F-1.

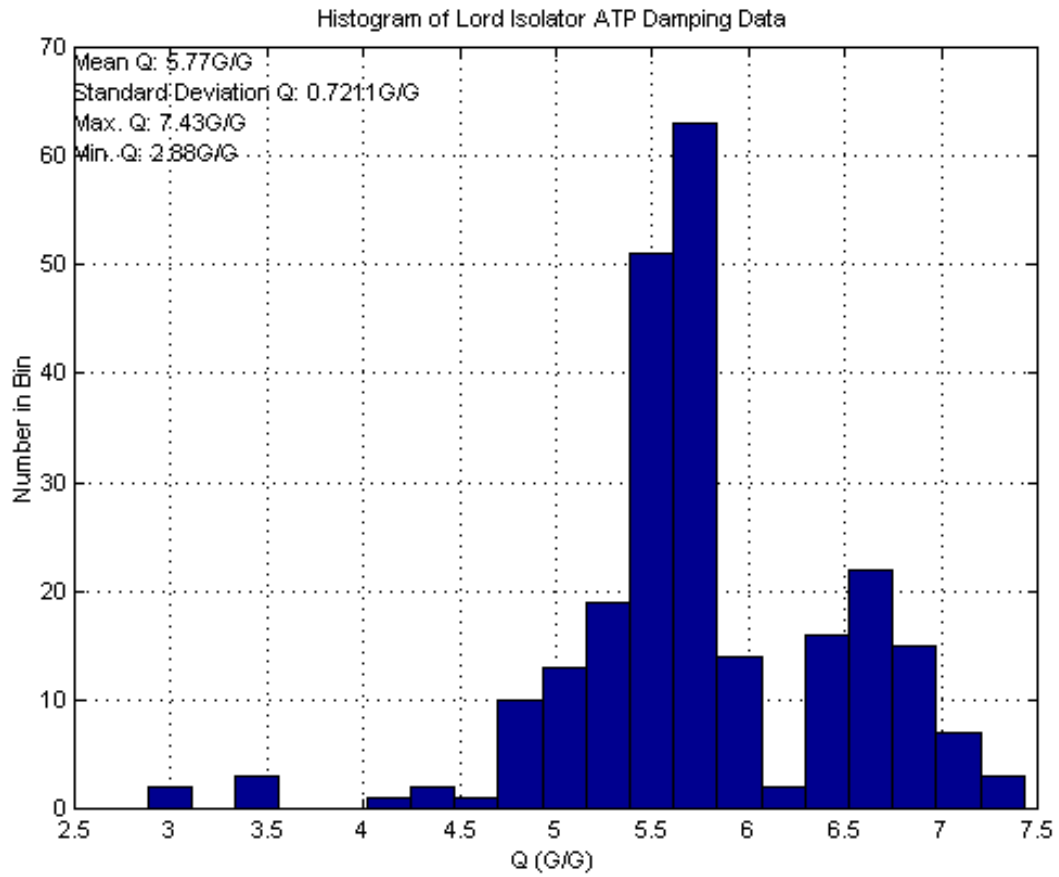


Figure F-2.

Reference:

ME File: 030-227A, Lord Isolator (156APLQ-8) General Random Vibration Transmissibility, 2002.

## APPENDIX G

### Flexible Confined Detonating Cord (FCDC)

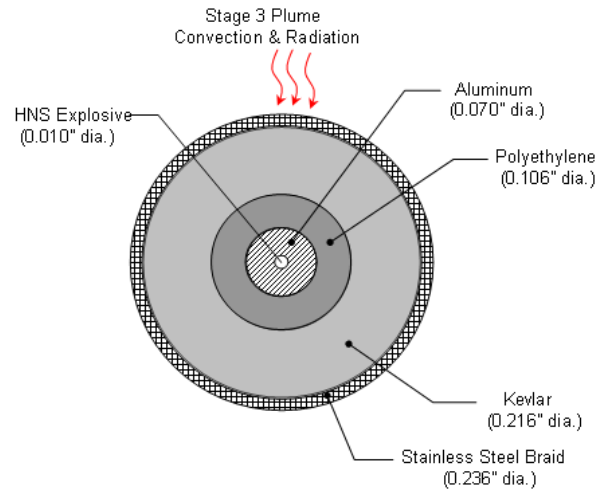


Figure G-1.

FCDC RESPONSE TEST 1 MODE 1  
20 Hz LP FILTERED

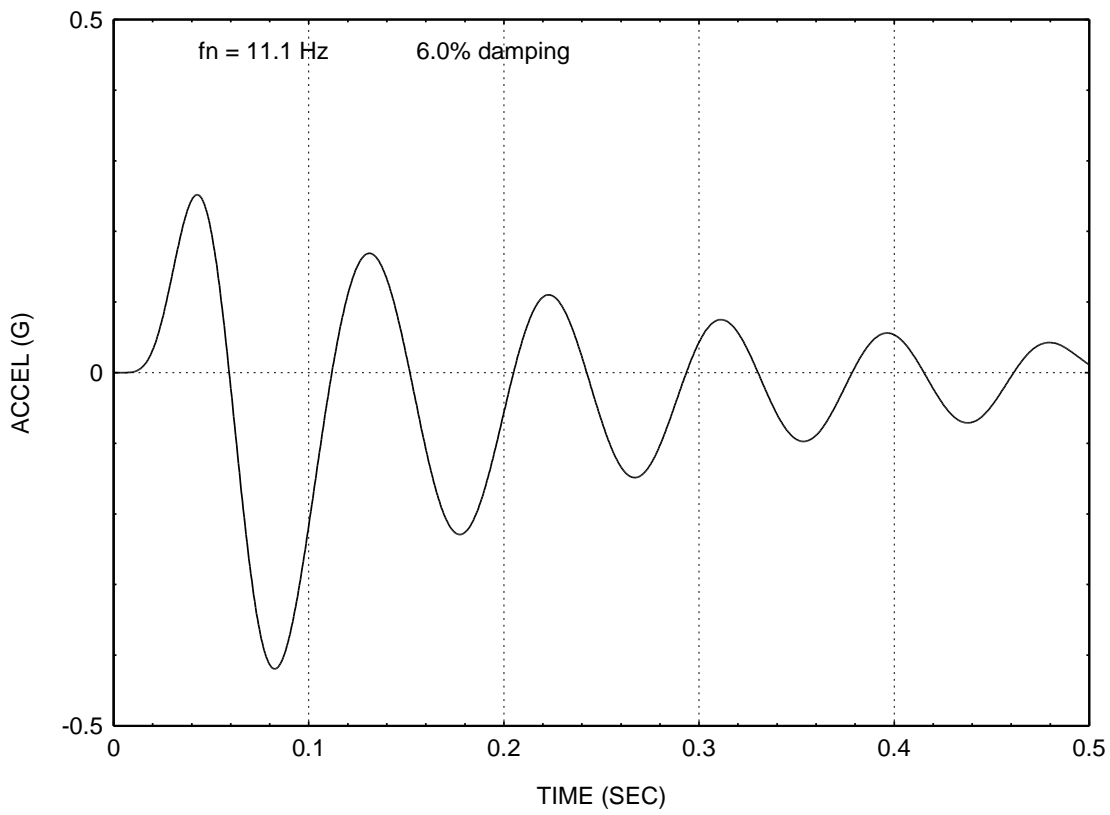


Figure G-2.

This was a test case for a particular configuration.

Other configurations were analyzed via FEA models in:

ME File: MISC 030-259, FCDC Vibration Frequency Analysis, 2003.

# APPENDIX H



Figure H-1.

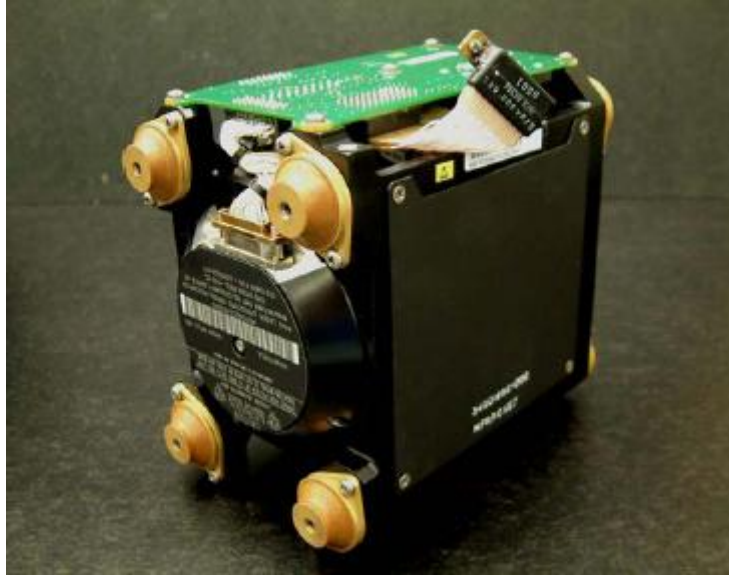


Figure H-2.

References:

ME File: 070-211A

ME File: 043-063



## APPENDIX I

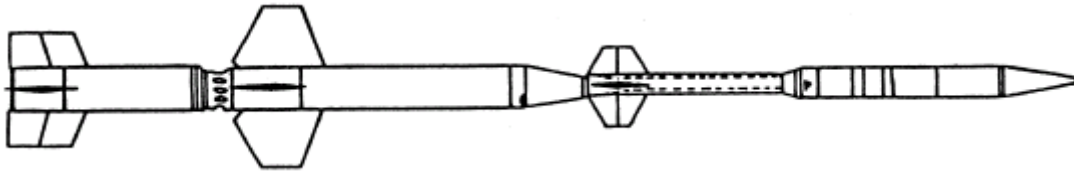


Figure I-1. HAVE Jeep VII F & G Talos-Sergeant-Hydac Vehicle

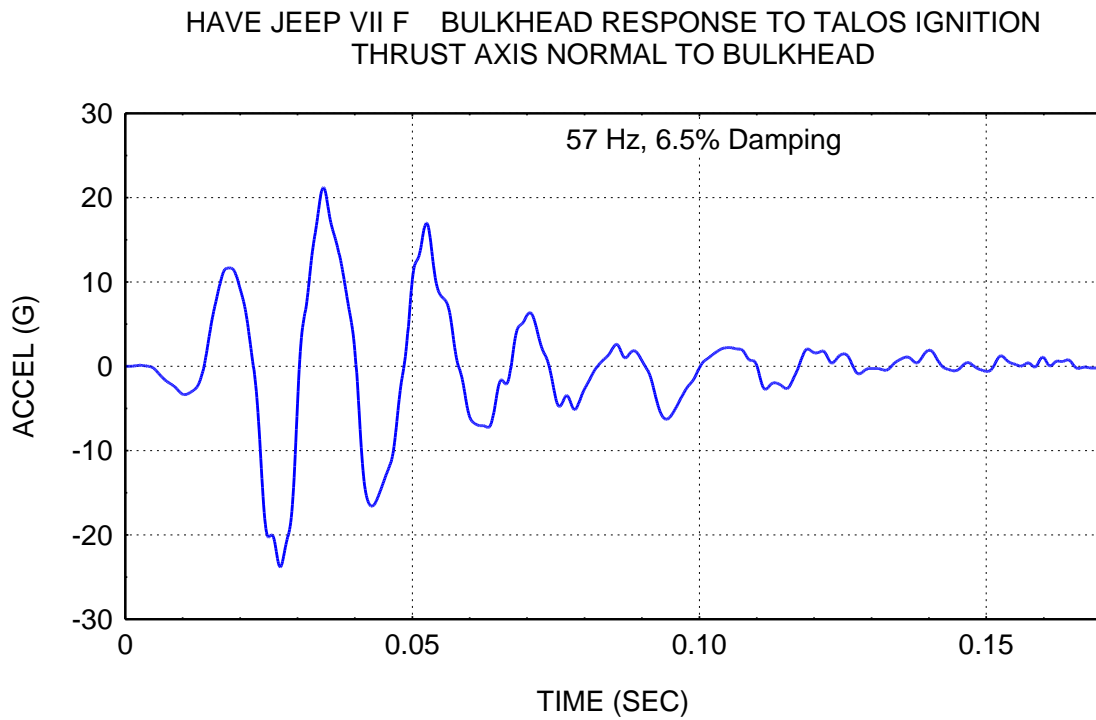


Figure I-2.

The bulkhead was circular, made from aluminum, homogeneous, with an 18 inch diameter. The data is from a flight in 1991.

The natural frequency and damping ratio were determined using a damped sine curve-fit.

# APPENDIX J

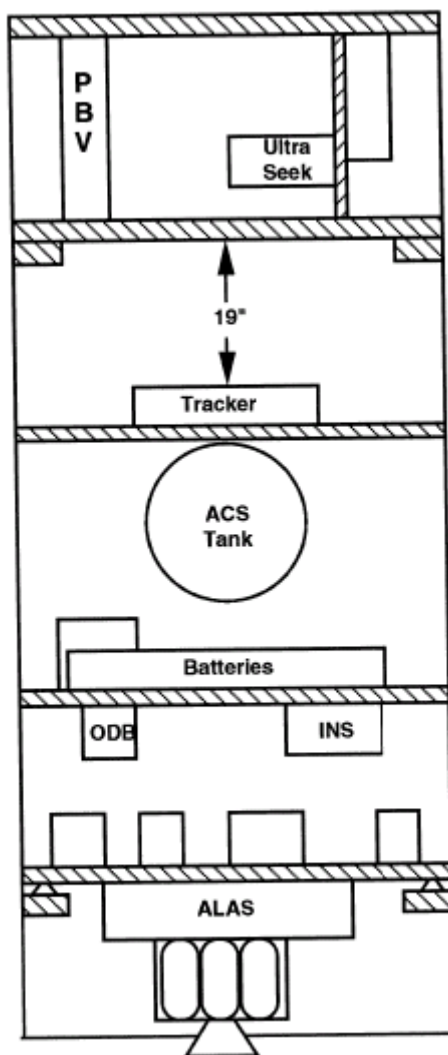


Figure J-1. Avionics Module with ALAS Bulkhead

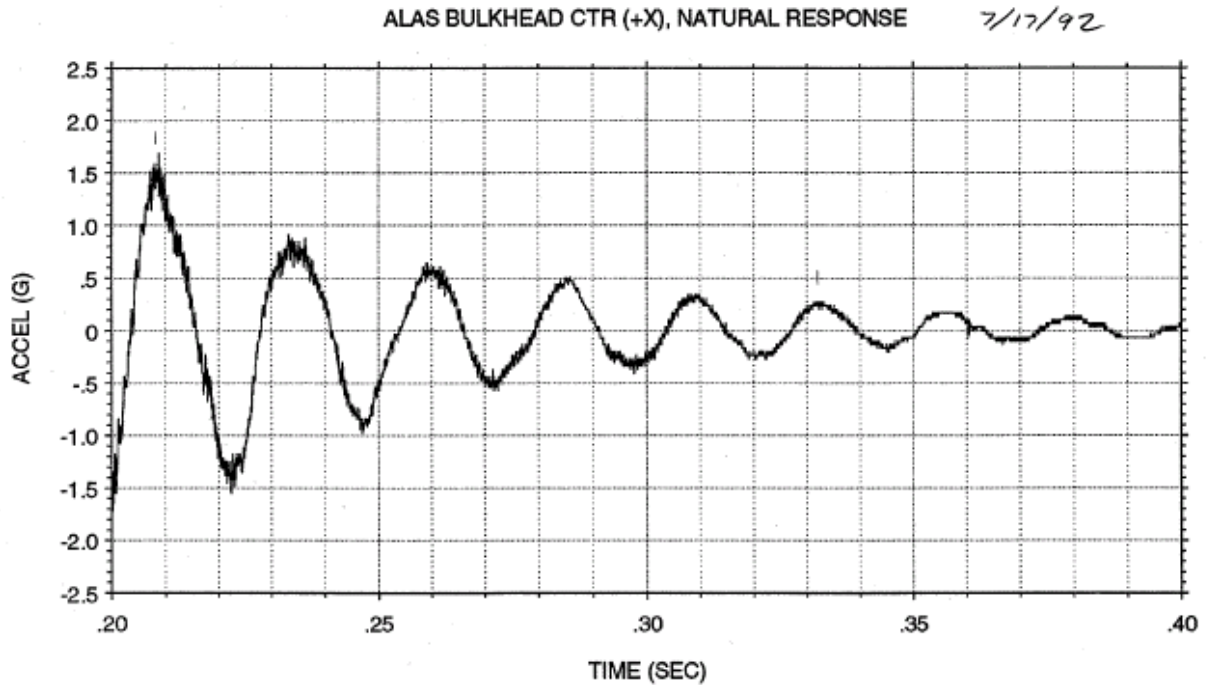


Figure J-2.

The bulkhead was circular, made from aluminum skins with a honeycomb core, and with a 38 inch diameter. It was mounted in a cylindrical avionics module. The module was then mounted to a shaker table. The shock pulse was applied in the axis normal to the bulkhead plane.

The data is from a shaker table shock test in 1992. The time segment shown represents the natural response immediately after the end of the input pulse. It is due to out-of-plane bending.

The natural frequency and damping ratio were determined using a damped sine curve-fit. The natural frequency is 40.0 Hz with 5.9% damping.