

ELECTRICAL-MECHANICAL ANALOGY FOR DYNAMIC SYSTEMS

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Table 1. Analogous Parameters

Mechanical System	Electrical Systems		
	Voltage-Force Analogy	Current-Force Analogy	
D'Alembert's principle	Kirchhoff's voltage law	Kirchhoff's current law	
Degree-of-freedom	Loop	Node	
Force Applied	Switch Closed	Switch Closed	
F Force	v Voltage	i Current	
m Mass	L Inductance	C Capacitance	
x Displacement	q Charge	$\phi = \int v dt$	
\dot{x} Velocity	i Loop Current	v Node voltage	
c Damping	R Resistance	1/R Conductance	
k Spring	1/C 1/Capacitance	1/L 1/Inductance	
Coupling Element	Element common to two loops	Element between nodes	

Impedance

Table 2. Electrical Impedance	
Element	Impedance
Capacitor	$Z_C = \frac{1}{j\omega C}$
Inductor	$Z_L = j\omega L$
Resistor	$Z_R = R$

Current-Force Analogy

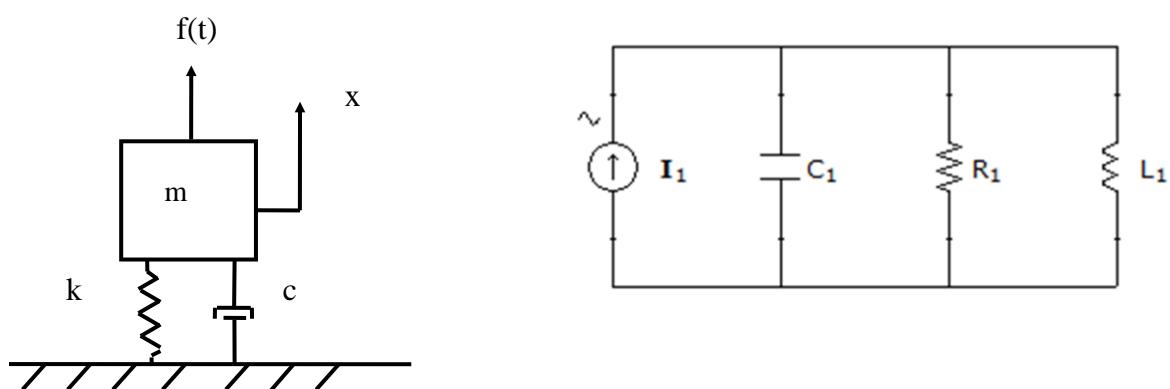


Figure 1. Equivalent Mechanical and Electrical Systems, SDOF System

The equation of motion for the mechanical oscillator is

$$m \frac{d^2x}{dt^2} + c \frac{dx}{dt} + kx = F(t) \quad (1)$$

Convert to velocity format.

$$m \frac{d}{dt} \left(\frac{dx}{dt} \right) + c \frac{dx}{dt} + k \int \left(\frac{dx}{dt} \right) dt = F(t) \quad (2)$$

Substitute the current-force analogy values from Table 1.

$$C \frac{dv}{dt} + \frac{1}{R} v + \frac{1}{L} \int v dt = i(t) \quad (3)$$

Take the derivative.

$$C \frac{d^2v}{dt^2} + \frac{1}{R} \frac{dv}{dt} + \frac{1}{L} v = \frac{d}{dt} i(t) \quad (4)$$

Voltage-Force Analogy

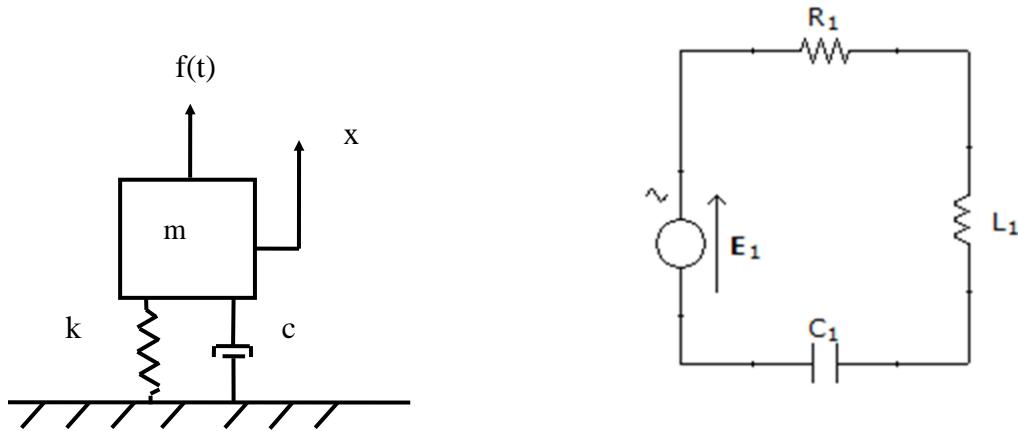


Figure 2. Equivalent Mechanical and Electrical Systems, SDOF System

Recall

$$m \frac{d}{dt} \left(\frac{dx}{dt} \right) + c \frac{dx}{dt} + k \int \left(\frac{dx}{dt} \right) dt = F(t) \quad (5)$$

Substitute the voltage-force analogy values from Table 1.

$$L \frac{di}{dt} + Ri + \frac{1}{C} \int i dt = v(t) \quad (6)$$

References

1. W. Seto, Mechanical Vibrations, McGraw-Hill, New York, 1964.
2. Cyril Harris, Shock and Vibration Handbook, 4th edition, McGraw-Hill, New York, 1995. See E. Hixson, Mechanical Impedance, Chapter 10.
3. T. Irvine, The Generalized Coordinate Method for Discrete Systems, Revision D, Vibrationdata, 2010.

APPENDIX A

Two-degree-of-freedom System

Voltage-Force Analogy

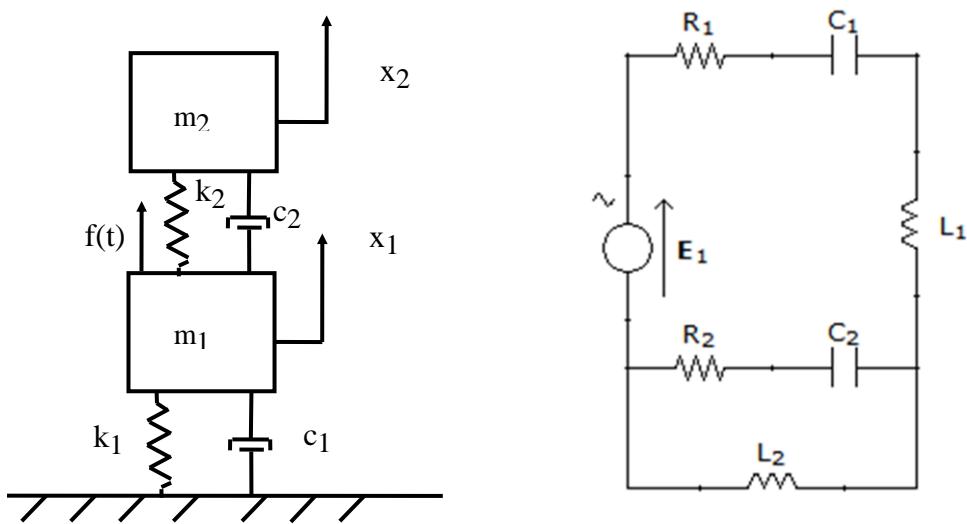


Figure A-1.

The equation of motion from Reference 3 is

$$\begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix} \begin{bmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{bmatrix} + \begin{bmatrix} c_1 + c_2 & -c_2 \\ -c_2 & c_2 \end{bmatrix} \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} + \begin{bmatrix} k_1 + k_2 & -k_2 \\ -k_2 & k_2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} f(t) \\ 0 \end{bmatrix}$$

(A-1)

The velocity form is

$$\begin{aligned}
 & \left[\begin{matrix} m_1 & 0 \\ 0 & m_2 \end{matrix} \right] \left\{ \frac{d}{dt} \begin{bmatrix} dx_1/dt \\ dx_2/dt \end{bmatrix} \right\} + \begin{bmatrix} c_1 + c_2 & -c_2 \\ -c_2 & c_2 \end{bmatrix} \begin{bmatrix} dx_1/dt \\ dx_2/dt \end{bmatrix} \\
 & + \begin{bmatrix} k_1 + k_2 & -k_2 \\ -k_2 & k_2 \end{bmatrix} \begin{bmatrix} \int \left(\frac{dx_1}{dt} \right) dt \\ \int \left(\frac{dx_2}{dt} \right) dt \end{bmatrix} = \begin{bmatrix} f(t) \\ 0 \end{bmatrix}
 \end{aligned} \tag{A-2}$$

Substitute the voltage-force analogy values from Table 1.

$$\begin{aligned}
 & \left[\begin{matrix} L_1 & 0 \\ 0 & L_2 \end{matrix} \right] \left[\begin{bmatrix} di_1/dt \\ di_2/dt \end{bmatrix} \right] + \begin{bmatrix} R_1 + R_2 & -R_2 \\ -R_2 & R_2 \end{bmatrix} \begin{bmatrix} i_1 \\ i_2 \end{bmatrix} \\
 & + \begin{bmatrix} 1/C_1 + 1/C_2 & -1/C_2 \\ -1/C_2 & C_2 \end{bmatrix} \begin{bmatrix} \int \left(\frac{di_1}{dt} \right) dt \\ \int \left(\frac{di_2}{dt} \right) dt \end{bmatrix} = \begin{bmatrix} v(t) \\ 0 \end{bmatrix}
 \end{aligned} \tag{A-3}$$

APPENDIX B

SDOF System, Base Excitation

Voltage-Force Analogy

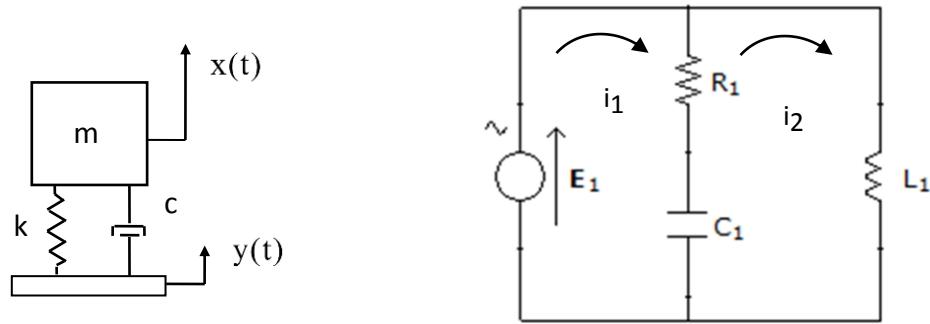


Figure B-1.

The equations of motion are

$$m \frac{d^2x}{dt^2} + c \left(\frac{dx}{dt} - \frac{dy}{dt} \right) + k(x - y) = 0 \quad (B-1)$$

and

$$-c \left(\frac{dx}{dt} - \frac{dy}{dt} \right) - k(x - y) = F(t) \quad (B-2)$$

where $F(t)$ is the force needed to maintain a prescribed $\frac{dy}{dt}$ or current by analogy.

The equations of motion in term of velocity are

$$m \frac{d}{dt} \left(\frac{dx}{dt} \right) + c \left(\frac{dx}{dt} - \frac{dy}{dt} \right) + k \left\{ \int \left(\frac{dx}{dt} \right) dt - \int \left(\frac{dy}{dt} \right) dt \right\} = 0 \quad (B-3)$$

and

$$-c \left(\frac{dx}{dt} - \frac{dy}{dt} \right) - k \left\{ \int \left(\frac{dx}{dt} \right) dt - \int \left(\frac{dy}{dt} \right) dt \right\} = F(t) \quad (B-4)$$

Substitute the current-force analogy values from Table 1.

$$L \frac{d}{dt} \left(\frac{di_1}{dt} \right) + R \left(\frac{di_1}{dt} - \frac{di_2}{dt} \right) + \frac{1}{C} \left\{ \int \left(\frac{di_1}{dt} \right) dt - \int \left(\frac{di_2}{dt} \right) dt \right\} = 0 \quad (B-5)$$

and

$$-R \left(\frac{di_1}{dt} - \frac{di_2}{dt} \right) - \frac{1}{C} \left\{ \int \left(\frac{di_1}{dt} \right) dt - \int \left(\frac{di_2}{dt} \right) dt \right\} = F(t) \quad (B-6)$$

Kirchhoff's voltage law, Loop Current Method

Solve for the current in Figure B-1.

$$E_1 + (i_1 - i_2) \left(R + \frac{1}{j\omega C} \right) = 0 \quad (B-7)$$

$$(i_1 - i_2) \left(R + \frac{1}{j\omega C} \right) - i_2 (j\omega L) = 0 \quad (B-8)$$

Let

$$Z_1 = \left(R + \frac{1}{j\omega C} \right) \quad (B-9)$$

$$Z_2 = j\omega L \quad (B-10)$$

$$E_1 + (i_1 - i_2)Z_1 = 0 \quad (B-11)$$

$$(i_1 - i_2)Z_1 - i_2 Z_2 = 0 \quad (B-12)$$

Simply as follows

$$i_1 Z_1 - i_2 Z_1 = -E_1 \quad (B-13)$$

$$i_1 Z_1 + i_2 (-Z_1 - Z_2) = 0 \quad (B-14)$$

Thus,

$$i_1 Z_1 = i_2 (Z_1 + Z_2) \quad (B-15)$$

$$i_2 (Z_1 - Z_2) - i_2 Z_1 = -E_1 \quad (B-16)$$

$$-i_2 Z_2 = -E_1 \quad (B-17)$$

$$i_2 = E_1 / Z_2 \quad (B-18)$$

$$i_1 = i_2 \frac{(Z_1 + Z_2)}{Z_1} \quad (B-19)$$

By substitution,

$$i_1 = E_1 \frac{(Z_1 + Z_2)}{Z_1 Z_2} \quad (B-20)$$

$$E_1 = i_1 \left[\frac{Z_1 Z_2}{Z_1 + Z_2} \right] \quad (B-21)$$

Thus the voltage source E_1 must be controlled to yield the desired i_1 .

By analogy, the force must be controlled to yield the desired base displacement and velocity.