

THE GENERALIZED COORDINATE METHOD FOR DISCRETE SYSTEMS SUBJECT TO BASE EXCITATION Revision B

By Tom Irvine
Email: tomirvine@aol.com

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Two-degree-of-freedom System

Consider a two-degree-of-freedom system subjected to base excitation, as shown in Figure 1. Free-body diagrams are shown in Figure 2.

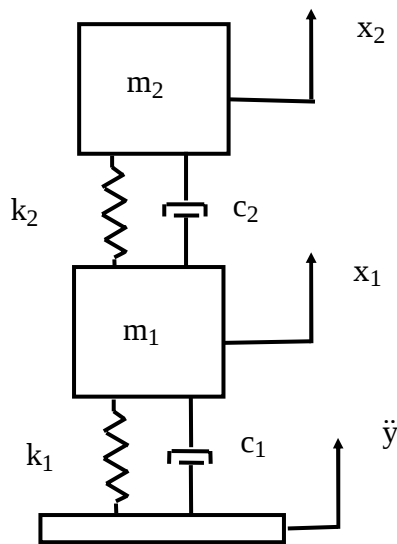


Figure 1.

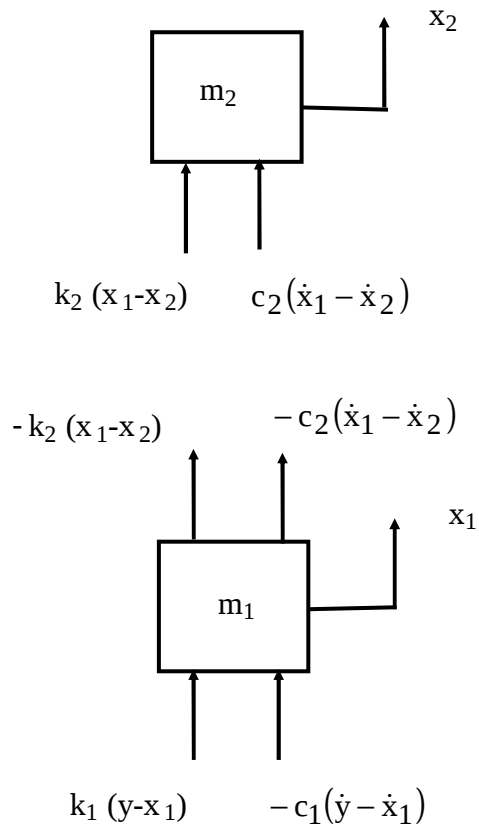


Figure 2.

Determine the equation of motion for mass 2.

$$\sum F = m_2 \ddot{x}_2 \quad (1)$$

$$m_2 \ddot{x}_2 = c_2(\dot{x}_1 - \dot{x}_2) + k_2(x_1 - x_2) \quad (2)$$

Define relative displacement terms.

$$z_2 = x_2 - y \quad (3)$$

$$x_2 = z_2 + y \quad (4)$$

$$z_1 = x_1 - y \quad (5)$$

$$x_1 = z_1 + y \quad (6)$$

Note that

$$x_1 - x_2 = z_1 - z_2 \quad (7)$$

Substitute the relative displacement terms into equation (2).

$$m_2 \ddot{z}_2 + m_2 \ddot{y} = c_2 (\dot{z}_1 - \dot{z}_2) + k_2 (z_1 - z_2) \quad (8)$$

$$m_2 \ddot{z}_2 + c_2 (-\dot{z}_1 + \dot{z}_2) + k_2 (-z_1 + z_2) = -m_2 \ddot{y} \quad (9)$$

$$m_2 \ddot{z}_2 + c_2 \dot{z}_2 - c_2 \dot{z}_1 + k_2 z_2 - k_2 z_1 = -m_2 \ddot{y} \quad (10)$$

Determine the equation of motion for mass 1.

$$\sum F = m_1 \ddot{x}_1 \quad (11)$$

$$m_1 \ddot{x}_1 = -c_2 (\dot{x}_1 - \dot{x}_2) + c_1 (\dot{y} - \dot{x}_1) - k_2 (x_1 - x_2) + k_1 (y - x_1) \quad (12)$$

$$m_1 \ddot{x}_1 = -c_2 (\dot{x}_1 - \dot{x}_2) + c_1 (\dot{y} - \dot{x}_1) - k_2 (x_1 - x_2) + k_1 (y - x_1) \quad (13)$$

$$m_1 \ddot{z}_1 + m_1 \ddot{y} = -c_2 (\dot{z}_1 - \dot{z}_2) + c_1 (\dot{y} - \dot{z}_1 - \dot{y}) - k_2 (z_1 - z_2) + k_1 (y - z_1 - y) \quad (14)$$

$$m_1 \ddot{z}_1 + m_1 \ddot{y} = -c_2 (\dot{z}_1 - \dot{z}_2) + c_1 (-\dot{z}_1) - k_2 (z_1 - z_2) + k_1 (-z_1) \quad (15)$$

$$m_1 \ddot{z}_1 + m_1 \ddot{y} = -c_2(\dot{z}_1 - \dot{z}_2) - c_1(\dot{z}_1) - k_2(z_1 - z_2) - k_1(z_1) \quad (16)$$

$$m_1 \ddot{z}_1 + c_2(\dot{z}_1 - \dot{z}_2) + c_1(\dot{z}_1) + k_2(z_1 - z_2) + k_1(z_1) = -m_1 \ddot{y} \quad (17)$$

$$m_1 \ddot{z}_1 + (c_1 + c_2)\dot{z}_1 - c_2\dot{z}_2 + (k_1 + k_2)z_1 - k_2 z_2 = -m_1 \ddot{y} \quad (18)$$

Assemble the equations in matrix form.

$$\begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix} \begin{bmatrix} \ddot{z}_1 \\ \ddot{z}_2 \end{bmatrix} + \begin{bmatrix} c_1 + c_2 & -c_2 \\ -c_2 & c_2 \end{bmatrix} \begin{bmatrix} \dot{z}_1 \\ \dot{z}_2 \end{bmatrix} + \begin{bmatrix} k_1 + k_2 & -k_2 \\ -k_2 & k_2 \end{bmatrix} \begin{bmatrix} z_1 \\ z_2 \end{bmatrix} = \begin{bmatrix} -m_1 \ddot{y} \\ -m_2 \ddot{y} \end{bmatrix} \quad (19)$$

Represent as

$$M\ddot{\bar{z}} + C\dot{\bar{z}} + K\bar{z} = F \quad (20)$$

$$M = \begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix} \quad (21)$$

$$C = \begin{bmatrix} c_1 + c_2 & -c_2 \\ -c_2 & c_2 \end{bmatrix} \quad (22)$$

$$K = \begin{bmatrix} k_1 + k_2 & -k_2 \\ -k_2 & k_2 \end{bmatrix} \quad (23)$$

$$F = \begin{bmatrix} -m_1 \ddot{y} \\ -m_2 \ddot{y} \end{bmatrix} \quad (24)$$

$$\bar{z} = \begin{bmatrix} z_1 \\ z_2 \end{bmatrix} \quad (25)$$

Consider the undamped, homogeneous form of equation (19).

$$\mathbf{M} \ddot{\bar{\mathbf{z}}} + \mathbf{K} \bar{\mathbf{z}} = \bar{\mathbf{0}} \quad (26)$$

Seek a solution of the form

$$\bar{\mathbf{z}} = \bar{\mathbf{q}} \exp(j\omega t) \quad (27)$$

The $\mathbf{q}$ vector is the generalized coordinate vector.

Note that

$$\dot{\bar{\mathbf{z}}} = j\omega \bar{\mathbf{q}} \exp(j\omega t) \quad (28)$$

$$\ddot{\bar{\mathbf{z}}} = -\omega^2 \bar{\mathbf{q}} \exp(j\omega t) \quad (29)$$

Substitute these equations into equation (26).

$$-\omega^2 \mathbf{M} \bar{\mathbf{q}} \exp(j\omega t) + \mathbf{K} \bar{\mathbf{q}} \exp(j\omega t) = \bar{\mathbf{0}} \quad (30)$$

$$\left\{ -\omega^2 \mathbf{M} + \mathbf{K} \right\} \bar{\mathbf{q}} \exp(j\omega t) = \bar{\mathbf{0}} \quad (31)$$

$$\left\{ -\omega^2 \mathbf{M} + \mathbf{K} \right\} \bar{\mathbf{q}} = \bar{\mathbf{0}} \quad (32)$$

$$\left\{ \mathbf{K} - \omega^2 \mathbf{M} \right\} \bar{\mathbf{q}} = \bar{\mathbf{0}} \quad (33)$$

Equation (28) is an example of a generalized eigenvalue problem. The eigenvalues can be found by setting the determinant equal to zero.

$$\det \left\{ \mathbf{K} - \omega^2 \mathbf{M} \right\} = 0 \quad (34)$$

$$\det \left\{ \begin{bmatrix} k_1 + k_2 & -k_2 \\ -k_2 & k_2 \end{bmatrix} - \omega^2 \begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix} \right\} = 0 \quad (35)$$

$$\det \begin{Bmatrix} (k_1 + k_2) - \omega^2 m_1 & -k_2 \\ -k_2 & k_2 - \omega^2 m_2 \end{Bmatrix} = 0 \quad (36)$$

$$\left[(k_1 + k_2) - \omega^2 m_1 \right] \left[k_2 - \omega^2 m_2 \right] - k_2^2 = 0 \quad (37)$$

$$-\omega^4 m_1 m_2 + \omega^2 [-m_2(k_1 + k_2) - m_1 k_2] - k_2^2 + k_2(k_1 + k_2) = 0 \quad (38)$$

$$-\omega^4 m_1 m_2 + \omega^2 [-m_2(k_1 + k_2) - m_1 k_2] - k_2^2 + k_1 k_2 + k_2^2 = 0 \quad (39)$$

$$-\omega^4 m_1 m_2 + \omega^2 [-m_2(k_1 + k_2) - m_1 k_2] + k_1 k_2 = 0 \quad (40)$$

The eigenvalues are the roots of the polynomial.

$$\omega_1^2 = \frac{-b - \sqrt{b^2 - 4ac}}{2a} \quad (41)$$

$$\omega_2^2 = \frac{-b + \sqrt{b^2 - 4ac}}{2a} \quad (42)$$

where

$$a = m_1 m_2 \quad (43)$$

$$b = [-m_2(k_1 + k_2) - m_1 k_2] \quad (44)$$

$$c = k_1 k_2 \quad (45)$$

The eigenvectors are found via the following equations.

$$\left\{ K - \omega_1^2 M \right\} \bar{q}_1 = \bar{0} \quad (46)$$

$$\left\{ K - \omega_2^2 M \right\} \bar{q}_2 = \bar{0} \quad (47)$$

where

$$\bar{q}_1 = \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} \quad (48)$$

$$\bar{q}_2 = \begin{bmatrix} w_1 \\ w_2 \end{bmatrix} \quad (49)$$

An eigenvector matrix Q can be formed. The eigenvectors are inserted in column format.

$$Q = [\bar{q}_1 \mid \bar{q}_2] \quad (50)$$

$$Q = \begin{bmatrix} v_1 & w_1 \\ v_2 & w_2 \end{bmatrix} \quad (51)$$

The eigenvectors represent orthogonal mode shapes.

Each eigenvector can be multiplied by an arbitrary scale factor. A mass-normalized eigenvector matrix $\hat{Q}$ can be obtained such that the following orthogonality relations are obtained.

$$\hat{Q}^T M \hat{Q} = I \quad (52)$$

$$\hat{Q}^T K \hat{Q} = \Omega \quad (53)$$

where

subscript T represents transpose

I is the identity matrix

Ω is a diagonal matrix of eigenvalues

Note that

$$\hat{Q} = \begin{bmatrix} \hat{v}_1 & \hat{w}_1 \\ \hat{v}_2 & \hat{w}_2 \end{bmatrix} \quad (54)$$

$$\hat{Q}^T = \begin{bmatrix} \hat{v}_1 & \hat{v}_2 \\ \hat{w}_1 & \hat{w}_2 \end{bmatrix} \quad (55)$$

Rigorous proof of the orthogonality relationships is beyond the scope of this tutorial. Further discussion is given in References 1 and 2.

Now define a modal coordinate $\eta(t)$ such that

$$\bar{z} = \hat{Q} \bar{\eta} \quad (56)$$

Substitute equation (56) into equation (20).

$$M \hat{Q} \bar{\ddot{\eta}} + C \hat{Q} \bar{\dot{\eta}} + K \hat{Q} \bar{\eta} = F \quad (57)$$

Premultiply by the transpose of the normalized eigenvector matrix.

$$\hat{Q}^T M \hat{Q} \bar{\ddot{\eta}} + \hat{Q}^T C \hat{Q} \bar{\dot{\eta}} + \hat{Q}^T K \hat{Q} \bar{\eta} = \hat{Q}^T F \quad (58)$$

The orthogonality relationships yield.

$$I \bar{\ddot{\eta}} + \hat{Q}^T C \hat{Q} \bar{\dot{\eta}} + \Omega \bar{\eta} = \hat{Q}^T F \quad (59)$$

Furthermore, the following assumption is made.

$$\hat{Q}^T C \hat{Q} \bar{\dot{\eta}} = \begin{bmatrix} 2\xi_1 \omega_1 & 0 \\ 0 & 2\xi_2 \omega_2 \end{bmatrix} \quad (60)$$

where ξ_i is the modal damping ratio for mode i .

$$\begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} \ddot{\eta}_1 \\ \ddot{\eta}_2 \end{bmatrix} + \begin{bmatrix} 2\xi_1 \omega_1 & 0 \\ 0 & 2\xi_2 \omega_2 \end{bmatrix} \begin{bmatrix} \dot{\eta}_1 \\ \dot{\eta}_2 \end{bmatrix} + \begin{bmatrix} \omega_1^2 & 0 \\ 0 & \omega_2^2 \end{bmatrix} \begin{bmatrix} \eta_1 \\ \eta_2 \end{bmatrix} = \begin{bmatrix} \hat{v}_1 & \hat{v}_2 \\ \hat{w}_1 & \hat{w}_2 \end{bmatrix} \begin{bmatrix} -m_1 \ddot{y} \\ -m_2 \ddot{y} \end{bmatrix} \quad (61)$$

The two equations are now decoupled in terms of the modal coordinate.

$$\ddot{\eta}_1 + 2\xi_1 \omega_1 \dot{\eta}_1 + \omega_1^2 \eta_1 = [-m_1 \hat{v}_1 - m_2 \hat{v}_2] \ddot{y} \quad (62)$$

$$\ddot{\eta}_2 + 2\xi_2 \omega_2 \dot{\eta}_2 + \omega_2^2 \eta_2 = [-m_1 \hat{w}_1 - m_2 \hat{w}_2] \ddot{y} \quad (63)$$

The equations can be solved in terms of Laplace transforms, or some other differential equation solution method.

Now consider the initial conditions. Recall

$$\bar{z} = \hat{Q} \bar{\eta} \quad (64)$$

Thus

$$\bar{z}(0) = \hat{Q} \bar{\eta}(0) \quad (65)$$

Premultiply by $\hat{Q}^T M$.

$$\hat{Q}^T M \bar{z}(0) = \hat{Q}^T M \hat{Q} \bar{\eta}(0) \quad (66)$$

Recall

$$\hat{Q}^T M \hat{Q} = I \quad (67)$$

$$\hat{Q}^T M \bar{z}(0) = I \bar{\eta}(0) \quad (68)$$

$$\hat{Q}^T M \bar{z}(0) = \bar{\eta}(0) \quad (69)$$

Finally, the transformed initial displacement matrix is

$$\bar{\eta}(0) = \hat{Q}^T M \bar{z}(0) \quad (70)$$

Similarly, the transformed initial velocity is

$$\dot{\bar{\eta}}(0) = \hat{Q}^T M \dot{\bar{z}}(0) \quad (71)$$

A basis for a solution is thus derived.

Harmonic Excitation

Assume that the net displacement and net velocity values are zero.

Now consider the special case of harmonic base excitation function.

$$\ddot{y}(t) = A \sin(\alpha t) \quad (72a)$$

$$\dot{y}(t) = \frac{-A}{\alpha} \cos(\alpha t) \quad (72b)$$

$$y(t) = \frac{-A}{\alpha^2} \sin(\alpha t) \quad (72c)$$

Solve for the steady-state response.

$$\ddot{\eta}_1 + 2\xi_1 \omega_1 \dot{\eta}_1 + \omega_1^2 \eta_1 = -A [m_1 \hat{v}_1 + m_2 \hat{v}_2] \sin(\alpha t) \quad (73)$$

$$\ddot{\eta}_2 + 2\xi_2 \omega_2 \dot{\eta}_2 + \omega_2^2 \eta_2 = -A [m_1 \hat{w}_1 + m_2 \hat{w}_2] \sin(\alpha t) \quad (74)$$

The solutions are taken from Reference (3).

$$\eta_1(t) = \frac{[m_1 \hat{v}_1 + m_2 \hat{v}_2] A}{\left[\left(\alpha^2 - \omega_1^2 \right)^2 + (2 \xi_1 \alpha \omega_1)^2 \right]} \left[(2 \xi_1 \alpha \omega_1) \cos(\alpha t) + \left(\alpha^2 - \omega_1^2 \right) \sin(\alpha t) \right]$$

(75a)

$$\eta_2(t) = \frac{[m_1 \hat{w}_1 + m_2 \hat{w}_2] A}{\left[\left(\alpha^2 - \omega_2^2 \right)^2 + (2 \xi_2 \alpha \omega_2)^2 \right]} \left[(2 \xi_2 \alpha \omega_2) \cos(\alpha t) + \left(\alpha^2 - \omega_2^2 \right) \sin(\alpha t) \right]$$

(75b)

The relative displacements can then be found from

$$\bar{z} = \hat{Q} \bar{\eta}$$

(76)

$$Q = \begin{bmatrix} \hat{v}_1 & \hat{w}_1 \\ \hat{v}_2 & \hat{w}_2 \end{bmatrix}$$

(77)

$$z_1(t) = \frac{\hat{v}_1 [m_1 \hat{v}_1 + m_2 \hat{v}_2] A}{\left[\left(\alpha^2 - \omega_1^2 \right)^2 + (2 \xi_1 \alpha \omega_1)^2 \right]} \left[(2 \xi_1 \alpha \omega_1) \cos(\alpha t) + \left(\alpha^2 - \omega_1^2 \right) \sin(\alpha t) \right]$$

$$+ \frac{\hat{w}_1 [m_1 \hat{w}_1 + m_2 \hat{w}_2] A}{\left[\left(\alpha^2 - \omega_2^2 \right)^2 + (2 \xi_2 \alpha \omega_2)^2 \right]} \left[(2 \xi_2 \alpha \omega_2) \cos(\alpha t) + \left(\alpha^2 - \omega_2^2 \right) \sin(\alpha t) \right]$$

(78)

$$\begin{aligned}
z_1(t) = & 2A\alpha \left\{ \frac{\hat{v}_1 [m_1 \hat{v}_1 + m_2 \hat{v}_2] (\xi_1 \omega_1)}{\left[\left(\alpha^2 - \omega_1^2 \right)^2 + (2\xi_1 \alpha \omega_1)^2 \right]} + \frac{\hat{w}_1 [m_1 \hat{w}_1 + m_2 \hat{w}_2] (\xi_2 \omega_2)}{\left[\left(\alpha^2 - \omega_2^2 \right)^2 + (2\xi_2 \alpha \omega_2)^2 \right]} \right\} \cos(\alpha t) \\
& + A \left\{ \frac{\hat{v}_1 [m_1 \hat{v}_1 + m_2 \hat{v}_2] (\alpha^2 - \omega_1^2)}{\left[\left(\alpha^2 - \omega_1^2 \right)^2 + (2\xi_1 \alpha \omega_1)^2 \right]} + \frac{\hat{w}_1 [m_1 \hat{w}_1 + m_2 \hat{w}_2] (\alpha^2 - \omega_2^2)}{\left[\left(\alpha^2 - \omega_2^2 \right)^2 + (2\xi_2 \alpha \omega_2)^2 \right]} \right\} \sin(\alpha t)
\end{aligned}
\tag{79}$$

$$\begin{aligned}
z_2(t) = & 2A\alpha \left\{ \frac{\hat{v}_2 [m_1 \hat{v}_1 + m_2 \hat{v}_2] (\xi_1 \omega_1)}{\left[\left(\alpha^2 - \omega_1^2 \right)^2 + (2\xi_1 \alpha \omega_1)^2 \right]} + \frac{\hat{w}_2 [m_1 \hat{w}_1 + m_2 \hat{w}_2] (\xi_2 \omega_2)}{\left[\left(\alpha^2 - \omega_2^2 \right)^2 + (2\xi_2 \alpha \omega_2)^2 \right]} \right\} \cos(\alpha t) \\
& + A \left\{ \frac{\hat{v}_2 [m_1 \hat{v}_1 + m_2 \hat{v}_2] (\alpha^2 - \omega_1^2)}{\left[\left(\alpha^2 - \omega_1^2 \right)^2 + (2\xi_1 \alpha \omega_1)^2 \right]} + \frac{\hat{w}_2 [m_1 \hat{w}_1 + m_2 \hat{w}_2] (\alpha^2 - \omega_2^2)}{\left[\left(\alpha^2 - \omega_2^2 \right)^2 + (2\xi_2 \alpha \omega_2)^2 \right]} \right\} \sin(\alpha t)
\end{aligned}
\tag{80}$$

The absolute displacements can then be found from

$$x_1 = z_1 + y \tag{81}$$

$$x_2 = z_2 + y \tag{82}$$

$$\begin{aligned}
x_1(t) = & 2A\alpha \left\{ \frac{\hat{v}_1 [m_1 \hat{v}_1 + m_2 \hat{v}_2] (\xi_1 \omega_1)}{\left[\left(\alpha^2 - \omega_1^2 \right)^2 + (2 \xi_1 \alpha \omega_1)^2 \right]} + \frac{\hat{w}_1 [m_1 \hat{w}_1 + m_2 \hat{w}_2] (\xi_2 \omega_2)}{\left[\left(\alpha^2 - \omega_2^2 \right)^2 + (2 \xi_2 \alpha \omega_2)^2 \right]} \right\} \cos(\alpha t) \\
& + A \left\{ \frac{\hat{v}_1 [m_1 \hat{v}_1 + m_2 \hat{v}_2] (\alpha^2 - \omega_1^2)}{\left[\left(\alpha^2 - \omega_1^2 \right)^2 + (2 \xi_1 \alpha \omega_1)^2 \right]} + \frac{\hat{w}_1 [m_1 \hat{w}_1 + m_2 \hat{w}_2] (\alpha^2 - \omega_2^2)}{\left[\left(\alpha^2 - \omega_2^2 \right)^2 + (2 \xi_2 \alpha \omega_2)^2 \right]} \right\} \sin(\alpha t) \\
& + \frac{-A}{\alpha^2} \sin(\alpha t)
\end{aligned} \tag{83}$$

$$\begin{aligned}
x_2(t) = & 2A\alpha \left\{ \frac{\hat{v}_2 [m_1 \hat{v}_1 + m_2 \hat{v}_2] (\xi_1 \omega_1)}{\left[\left(\alpha^2 - \omega_1^2 \right)^2 + (2 \xi_1 \alpha \omega_1)^2 \right]} + \frac{\hat{w}_2 [m_1 \hat{w}_1 + m_2 \hat{w}_2] (\xi_2 \omega_2)}{\left[\left(\alpha^2 - \omega_2^2 \right)^2 + (2 \xi_2 \alpha \omega_2)^2 \right]} \right\} \cos(\alpha t) \\
& + A \left\{ \frac{\hat{v}_2 [m_1 \hat{v}_1 + m_2 \hat{v}_2] (\alpha^2 - \omega_1^2)}{\left[\left(\alpha^2 - \omega_1^2 \right)^2 + (2 \xi_1 \alpha \omega_1)^2 \right]} + \frac{\hat{w}_2 [m_1 \hat{w}_1 + m_2 \hat{w}_2] (\alpha^2 - \omega_2^2)}{\left[\left(\alpha^2 - \omega_2^2 \right)^2 + (2 \xi_2 \alpha \omega_2)^2 \right]} \right\} \sin(\alpha t) \\
& + \frac{-A}{\alpha^2} \sin(\alpha t)
\end{aligned} \tag{84}$$

The velocity and acceleration terms can be found by taking derivatives.

References

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3. T. Irvine, Response of a Single-degree-of-freedom System Subjected to a Classical Pulse Base Excitation, Vibrationdata Publications, 1999.