FREE VIBRATION OF A SEMI-DEFINITE SYSTEM SUBJECTED TO INITIAL CONDITIONS

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Two-degree-of-freedom System

Consider a two-degree-of-freedom system, as shown in Figure 1.

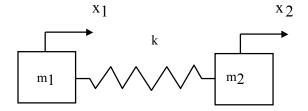


Figure 1.

The dashpot element between the masses is omitted for brevity.

The equation of motion from Reference 1 is

$$\begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix} \begin{bmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{bmatrix} + \begin{bmatrix} c & -c \\ -c & c \end{bmatrix} \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} + \begin{bmatrix} k & -k \\ -k & k \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$
(1)

Represent as

$$M \ddot{x} + C \bar{x} + K \bar{x} = F$$
⁽²⁾

$$\mathbf{M} = \begin{bmatrix} \mathbf{m}_1 & \mathbf{0} \\ \mathbf{0} & \mathbf{m}_2 \end{bmatrix} \tag{3}$$

$$C = \begin{bmatrix} c & -c \\ -c & c \end{bmatrix}$$
(4)

$$\mathbf{K} = \begin{bmatrix} \mathbf{k} & -\mathbf{k} \\ -\mathbf{k} & \mathbf{k} \end{bmatrix} \tag{5}$$

$$\mathbf{F} = \begin{bmatrix} \mathbf{0} \\ \mathbf{0} \end{bmatrix} \tag{6}$$

Consider the undamped, homogeneous form of equation (2).

$$M \ \overline{\ddot{x}} + K \ \overline{x} = \overline{0} \tag{7}$$

Seek a solution of the form

$$\overline{\mathbf{x}} = \overline{\mathbf{q}} \exp(\mathbf{j}\omega \mathbf{t}) \tag{8}$$

The q vector is the generalized coordinate vector.

Note that

$$\bar{\mathbf{x}} = \mathbf{j}\boldsymbol{\omega}\,\overline{\mathbf{q}}\,\exp(\mathbf{j}\boldsymbol{\omega}\mathbf{t})\tag{9}$$

$$\overline{\ddot{x}} = -\omega^2 \,\overline{q} \exp(j\omega t) \tag{10}$$

Substitute these equations into equation (2).

$$-\omega^2 M \ \overline{q} \exp(j\omega t) + K \ \overline{q} \exp(j\omega t) = \overline{0}$$
(11)

$$\left\{-\omega^2 M + K\right\} \overline{q} \exp(j\omega t) = \overline{0}$$
(12)

$$\left\{-\omega^2 M + K\right\} \overline{q} = \overline{0} \tag{13}$$

$$\left\{ K - \omega^2 M \right\} \overline{q} = \overline{0} \tag{14}$$

Equation (14) is an example of a generalized eigenvalue problem. The eigenvalues can be found by setting the determinant equal to zero.

$$\det\left\{K - \omega^2 M\right\} = 0 \tag{15}$$

$$\det\left\{ \begin{bmatrix} k_2 & -k_2 \\ -k_2 & k_2 \end{bmatrix} - \omega^2 \begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix} \right\} = 0$$
(16)

$$\det \begin{cases} k_2 - \omega^2 m_1 & -k_2 \\ -k_2 & k_2 - \omega^2 m_2 \end{cases} = 0$$
(17)

$$\left[k_{2} - \omega^{2}m_{1}\right]\left[k_{2} - \omega^{2}m_{2}\right] - k_{2}^{2} = 0$$
(18)

$$\omega^4 m_1 m_2 - \omega^2 [m_2 k_2 + m_1 k_2] = 0$$
⁽¹⁹⁾

$$\omega_{l} = 0 \tag{20}$$

$$\omega^2 m_1 m_2 - [m_2 k_2 + m_1 k_2] = 0 \tag{21}$$

$$\omega^2 = \frac{m_2 k_2 + m_1 k_2}{m_1 m_2} \tag{22}$$

$$\omega_2 = \sqrt{\frac{m_2 k_2 + m_1 k_2}{m_1 m_2}}$$
(23)

The eigenvectors are found via the following equations.

$$\mathbf{K} \ \overline{\mathbf{q}} \ \mathbf{1} = \overline{\mathbf{0}} \tag{24}$$

$$\left\{K - \omega_2^2 M\right\} \overline{q}_2 = \overline{0}$$
⁽²⁵⁾

where

$$\overline{\mathbf{q}}_1 = \begin{bmatrix} \mathbf{v}_1 \\ \mathbf{v}_2 \end{bmatrix} \tag{26}$$

$$\overline{q}_2 = \begin{bmatrix} w_1 \\ w_2 \end{bmatrix}$$
(27)

An eigenvector matrix Q can be formed. The eigenvectors are inserted in column format.

$$Q = \begin{bmatrix} \overline{q}_1 | \overline{q}_2 \end{bmatrix}$$
(28)

$$Q = \begin{bmatrix} v_1 & w_1 \\ v_2 & w_2 \end{bmatrix}$$
(29)

The eigenvectors represent orthogonal mode shapes.

Each eigenvector can be multiplied by an arbitrary scale factor. A mass-normalized eigenvector matrix \hat{Q} can be obtained such that the following orthogonality relations are obtained.

$$\hat{\mathbf{Q}}^{\mathrm{T}} \mathbf{M} \,\hat{\mathbf{Q}} = \mathbf{I} \tag{30}$$

$$\hat{\mathbf{Q}}^{\mathrm{T}} \mathbf{K} \, \hat{\mathbf{Q}} = \mathbf{\Omega} \tag{31}$$

where

superscript T represents transpose

I is the identity matrix

 Ω is a diagonal matrix of eigenvalues

Note that

$$Q = \begin{bmatrix} \hat{v}_1 & \hat{w}_1 \\ \hat{v}_2 & \hat{w}_2 \end{bmatrix}$$
(32)

$$Q^{\mathrm{T}} = \begin{bmatrix} \hat{v}_1 & \hat{v}_2\\ \hat{w}_1 & \hat{w}_2 \end{bmatrix}$$
(33)

Rigorous proof of the orthogonality relationships is beyond the scope of this tutorial. Further discussion is given in the references.

Now define a modal coordinate $\eta(t)$ such that

$$\overline{\mathbf{x}} = \hat{\mathbf{Q}}\,\overline{\boldsymbol{\eta}} \tag{34}$$

Substitute equation (34) into equation (2).

$$M\hat{Q}\,\overline{\ddot{\eta}} + C\hat{Q}\,\overline{\dot{\eta}} + K\hat{Q}\,\overline{\eta} = F$$
(35)

Premultiply by the transpose of the normalized eigenvector matrix.

$$\hat{Q}^{T}M\hat{Q}\,\overline{\eta} + \hat{Q}^{T}C\hat{Q}\,\overline{\eta} + \hat{Q}^{T}K\hat{Q}\,\overline{\eta} = \hat{Q}^{T}F$$
(36)

The orthogonality relationships yield

$$I \ \overline{\ddot{\eta}} + \hat{Q}^{T} C \hat{Q} \, \overline{\dot{\eta}} + \Omega \, \overline{\eta} = \hat{Q}^{T} F$$
(37)

Furthermore, the following assumption is made.

$$\hat{\mathbf{Q}}^{\mathrm{T}} \mathbf{C} \hat{\mathbf{Q}} \,\overline{\dot{\boldsymbol{\eta}}} = \begin{bmatrix} 0 & 0 \\ 0 & 2\xi_2 \,\omega_2 \end{bmatrix} \tag{38}$$

where ξ_i is the modal damping ratio for mode i.

$$\begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} \ddot{\eta}_1 \\ \ddot{\eta}_2 \end{bmatrix} + \begin{bmatrix} 0 & 0 \\ 0 & 2\xi_2 \omega_2 \end{bmatrix} \begin{bmatrix} \dot{\eta}_1 \\ \dot{\eta}_2 \end{bmatrix} + \begin{bmatrix} 0 & 0 \\ 0 & \omega_2^2 \end{bmatrix} \begin{bmatrix} \eta_1 \\ \eta_2 \end{bmatrix} = \begin{bmatrix} \hat{v}_1 & \hat{v}_2 \\ \hat{w}_1 & \hat{w}_2 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$
(39)

$$\begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} \ddot{\eta}_1 \\ \ddot{\eta}_2 \end{bmatrix} + \begin{bmatrix} 0 & 0 \\ 0 & 2\xi_2 \omega_2 \end{bmatrix} \begin{bmatrix} \dot{\eta}_1 \\ \dot{\eta}_2 \end{bmatrix} + \begin{bmatrix} 0 & 0 \\ 0 & \omega_2^2 \end{bmatrix} \begin{bmatrix} \eta_1 \\ \eta_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$
(40)

The two equations are now decoupled in terms of the modal coordinate.

$$\ddot{\eta}_1 = 0 \tag{41}$$

$$\ddot{\eta}_2 + 2\xi_2 \,\omega_2 \,\dot{\eta}_2 + \omega_2^2 \,\eta_2 = 0 \tag{42}$$

The solution to the first is

$$\eta_1(t) = \dot{\eta}_1(0)t + \eta_1(0) \tag{43a}$$

$$\eta_1(t) = \dot{\eta}_1(0)$$
 (43b)

The following equation is obtained via Reference 5.

$$\eta_{2}(t) = \exp(-\xi_{2}\omega_{2}t) \left\{ \eta_{2}(0)\cos(\omega_{d2}t) + \frac{1}{\omega_{d2}} [\xi_{2}\omega_{2}\eta_{2}(0) + \dot{\eta}_{2}(0)]\sin(\omega_{d2}t) \right\}$$
(44)

$$\dot{\eta}_{2}(t) = -\xi_{2} \omega_{2} \exp(-\xi_{2} \omega_{2} t) \left\{ \eta_{2}(0) \cos(\omega_{d2} t) + \frac{1}{\omega_{d2}} [\xi_{2} \omega_{2} \eta_{2}(0) + \dot{\eta}_{2}(0)] \sin(\omega_{d2} t) \right\} \\ + \omega_{d2} \exp(-\xi_{2} \omega_{2} t) \left\{ -\eta_{2}(0) \sin(\omega_{d2} t) + \frac{1}{\omega_{d2}} [\xi_{2} \omega_{2} \eta_{2}(0) + \dot{\eta}_{2}(0)] \cos(\omega_{d2} t) \right\}$$

$$(45)$$

$$\dot{\eta}_{2}(t) = -\xi_{2} \omega_{2} \eta_{2}(t) + \omega_{d2} \exp(-\xi_{2} \omega_{2} t) \left\{ -\eta_{2}(0) \sin(\omega_{d2} t) + \frac{1}{\omega_{d2}} [\xi_{2} \omega_{2} \eta_{2}(0) + \dot{\eta}_{2}(0)] \cos(\omega_{d2} t) \right\}$$
(46)

$$\ddot{\eta}_{2}(t) = -2\xi_{2}\omega_{2}\dot{\eta}_{2}(t) - \omega_{2}^{2}\eta_{2}(t)$$
(47)

Recall

$$\overline{\mathbf{x}} = \hat{\mathbf{Q}}\,\overline{\boldsymbol{\eta}} \tag{48}$$

The displacements are

 $x_1(t) = v_1 \eta_1(t) + w_1 \eta_2(t)$ (49)

$$x_{2}(t) = v_{2} \eta_{1}(t) + w_{2} \eta_{2}(t)$$
(50)

The velocities are

$$\dot{x}_1(t) = v_1 \dot{\eta}_1(t) + w_1 \dot{\eta}_2(t)$$
(51)

$$\dot{\mathbf{x}}_{2}(t) = \mathbf{v}_{2} \dot{\eta}_{1}(t) + \mathbf{w}_{2} \dot{\eta}_{2}(t)$$
 (52)

$$\dot{x}_1(t) = v_1 \dot{\eta}_1(0) t + w_1 \dot{\eta}_2(t)$$
(53)

$$\dot{\mathbf{x}}_{2}(t) = \mathbf{v}_{2}\dot{\eta}_{1}(0)t + \mathbf{w}_{2}\dot{\eta}_{2}(t)$$
 (54)

The accelerations are

$$\ddot{x}_{1}(t) = v_{1} \ddot{\eta}_{1}(t) + w_{1} \ddot{\eta}_{2}(t)$$
(55)

$$\ddot{x}_{2}(t) = v_{2} \ddot{\eta}_{1}(t) + w_{2} \ddot{\eta}_{2}(t)$$
(56)

Recall equation (41). The accelerations simplify to

$$\ddot{x}_1(t) = w_1 \ddot{\eta}_2(t)$$
 (57)

$$\ddot{x}_2(t) = w_2 \ddot{\eta}_2(t)$$
 (58)

Now consider the initial conditions. Recall

$$\overline{\mathbf{x}} = \hat{\mathbf{Q}}\,\overline{\mathbf{\eta}} \tag{59}$$

Thus

$$\overline{\mathbf{x}}(0) = \hat{\mathbf{Q}} \,\overline{\boldsymbol{\eta}}(0) \tag{60}$$

Premultiply by $\hat{Q}^T M$.

$$\hat{\mathbf{Q}}^{\mathrm{T}} \mathbf{M} \,\overline{\mathbf{x}}(0) = \hat{\mathbf{Q}}^{\mathrm{T}} \,\mathbf{M} \,\hat{\mathbf{Q}} \,\,\overline{\boldsymbol{\eta}}(0) \tag{61}$$

Recall

$$\hat{Q}^{T} M \hat{Q} = I \tag{62}$$

$$\hat{Q}^{T} M \overline{x}(0) = I \overline{\eta}(0)$$
(63)

$$\hat{\mathbf{Q}}^{\mathrm{T}} \mathbf{M} \,\overline{\mathbf{x}}(0) = \overline{\mathbf{\eta}}(0) \tag{64}$$

Finally, the transformed initial displacement matrix is

$$\overline{\eta}(0) = \hat{Q}^{T} M \overline{x}(0)$$
(65)

Similarly, the transformed initial velocity is

$$\overline{\dot{\eta}}(0) = \hat{Q}^{T} M \overline{\dot{x}}(0)$$
(66)

A basis for a solution is thus derived.

<u>References</u>

- 1. T. Irvine, Semi-Definite System Examples, Vibrationdata, 2008.
- 2. Bathe, Finite Element Procedures in Engineering Analysis, Prentice-Hall, New Jersey, 1982. Section 12.3.1.
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- 4. T. Irvine, Response of a Single-degree-of-freedom System Subjected to a Classical Pulse Base Excitation, Vibrationdata, 1999.
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