CALCULATING TRANSFER FUNCTIONS FROM NORMAL MODES Revision E

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Variables

F	Excitation frequency
fr	Natural frequency for mode <i>r</i>
Ν	Total degrees-of-freedom
H _{ij} (f)	The steady state displacement at coordinate i due to a harmonic force excitation only at coordinate j
ξr	Damping ratio for mode <i>r</i>
φ _{ir}	Mass-normalized eigenvector for physical coordinate i and mode number r
ω	Excitation frequency (rad/sec)
ω _r	Natural frequency (rad/sec) for mode <i>r</i>

Receptance

The steady-state displacement at coordinate i due to a harmonic force excitation only at coordinate j is:

$$H_{ij}(f) = \sum_{r=1}^{N} \left\{ \frac{\phi_{ir} \phi_{jr}}{\omega_r^2} \frac{1}{\left(1 - \rho_r^2\right) + \hat{j}\left(2\xi_r\rho_r\right)} \right\}$$
(1)

where

$$\rho_{\rm r} = f / f_{\rm r} \tag{2}$$

$$\hat{j} = \sqrt{-1} \tag{3}$$

Note that the phase angle is typically represented as the angle by which force leads displacement. In terms of a C++ or Matlab type equation, the phase angle would be

$$Phase = -atan2(imag(H), real(H))$$
(4)

Note that both the phase and the transfer function vary with frequency.

A more formal equation is

Phase(f) = - arctan
$$\left\{ \frac{imag(H_{ij}(f))}{real(H_{ij}(f))} \right\}$$
 (5)

<u>Mobility</u>

The steady-state velocity at coordinate i due to a harmonic force excitation only at coordinate j is

$$H_{ij}(f) = j\omega \sum_{r=1}^{N} \left\{ \frac{\phi_{ir} \phi_{jr}}{\omega_r^2} \frac{1}{\left(1 - \rho_r^2\right) + \hat{j} \left(2\xi_r \rho_r\right)} \right\}$$
(6)

Accelerance

The steady-state acceleration at coordinate i due to a harmonic force excitation only at coordinate j is

$$H_{ij}(f) = -\omega^2 \sum_{r=1}^{N} \left\{ \frac{\phi_{ir} \phi_{jr}}{\omega_r^2} \frac{1}{\left(1 - \rho_r^2\right) + \hat{j} \left(2\xi_r \rho_r\right)} \right\}$$
(7)

Relative Displacement

Consider two translational degrees-of-freedom i and j. A force is applied at degree-of-freedom k.

The steady-state relative displacement transfer function R_{ij} between *i* and *j* due to an applied force at *k* is

$$R_{ij} = H_{ik}(f) - H_{jk}(f)$$

$$= \sum_{r=1}^{N} \left\{ \frac{\phi_{ir} \phi_{kr}}{\omega_{r}^{2}} \frac{1}{(1 - \rho_{r}^{2}) + \hat{j} (2\xi_{r}\rho_{r})} \right\} - \sum_{r=1}^{N} \left\{ \frac{\phi_{jr} \phi_{kr}}{\omega_{r}^{2}} \frac{1}{(1 - \rho_{r}^{2}) + \hat{j} (2\xi_{r}\rho_{r})} \right\}$$
(8)

$$R_{ij} = \sum_{r=1}^{N} \left\{ \frac{\left(\phi_{ir} - \phi_{jr}\right)\phi_{kr}}{\omega_{r}^{2}} \frac{1}{\left(1 - \rho_{r}^{2}\right) + \hat{j}\left(2\xi_{r}\rho_{r}\right)} \right\}$$
(9)

The steady-state relative displacement transfer function R_{ij} between *i* and *j* due to an applied force at *k* is

$$R_{ij} = H_{ik}(f) - H_{jk}(f)$$

$$= \sum_{r=1}^{N} \left\{ \frac{\phi_{ir} \phi_{kr}}{\omega_{r}^{2}} \frac{1}{(1 - \rho_{r}^{2}) + \hat{j} (2\xi_{r}\rho_{r})} \right\} - \sum_{r=1}^{N} \left\{ \frac{\phi_{jr} \phi_{kr}}{\omega_{r}^{2}} \frac{1}{(1 - \rho_{r}^{2}) + \hat{j} (2\xi_{r}\rho_{r})} \right\}$$
(10)

$$R_{ij} = \sum_{r=1}^{N} \left\{ \frac{\left(\phi_{ir} - \phi_{jr}\right)\phi_{kr}}{\omega_{r}^{2}} \frac{\left(1 - \rho_{r}^{2}\right)}{\left(1 - \rho_{r}^{2}\right)^{2} + (2\xi_{r}\rho_{r})^{2}} \right\}$$
$$-j\sum_{r=1}^{N} \left\{ \frac{\left(\phi_{ir} - \phi_{jr}\right)\phi_{kr}}{\omega_{r}^{2}} \frac{(2\xi_{r}\rho_{r})}{\left(1 - \rho_{r}^{2}\right)^{2} + (2\xi_{r}\rho_{r})^{2}} \right\}$$
(11)

<u>Reference</u>

1. R. Craig & A. Kurdila, Fundamentals of Structural Dynamics, Second Edition, Wiley, New Jersey, 2006.

APPENDIX A

EXAMPLE 1



Consider the system in Figure A-1. Assign the values in Table A-1.

Table A-1. Parameters				
Variable	Value	Unit		
m	1.0	lbf sec^2/in		
k	3.946e+05	lbf/in		
Damping Ratio	0.05	-		

TRANSFER FUNCTION PHASE H11



Figure A-1.

This is the phase angle by which the force leads the response.



Figure A-2.

APPENDIX B

EXAMPLE 2

Normal Modes Analysis



Figure B-1.

Consider the system in Figure B-1. Assign the values in Table B-1.

Table B-1. Parameters				
Variable	Value	Unit		
m ₁	3.0	lbf sec^2/in		
m ₂	2.0	lbf sec^2/in		
k ₁	400,000	lbf/in		
k ₂	300,000	lbf/in		
k ₃	100,000	lbf/in		

Furthermore, assume

- 1. Each mode has a damping value of 5%.
- 2. Zero initial conditions

The homogeneous, undamped problem is

$$\begin{bmatrix} 3 & 0 \\ 0 & 2 \end{bmatrix} \begin{bmatrix} \ddot{z}_1 \\ \ddot{z}_2 \end{bmatrix} + \begin{bmatrix} 500,000 & -100,000 \\ -100,000 & 400,000 \end{bmatrix} \begin{bmatrix} z_1 \\ z_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$
(B-3)

The eigenvalue problem is

$$\begin{bmatrix} 500,000 - 2\omega^2 & -100,000 \\ -100,000 & 400,000 - \omega^2 \end{bmatrix} \begin{bmatrix} q_1 \\ q_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$
(B-4)

The analysis is performed using Matlab script: transfer_from_modes.m

```
>> transfer_from_modes
 transfer from modes.m ver 1.4 June 4, 2010
by Tom Irvine
 This program calculates a transfer function (displacement/force)
 for each degree-of-freedom in a system based on the mode shapes,
 natural frequencies, and damping ratios.
 Select input method
  1=mass & stiffness matrices
  2=natural frequencies and mass-normalized eigenvectors
 1
 Select output metric
  1=displacement/force
  2=velocity/force
  3=acceleration/force
 1
 Enter the mass matrix name: mm
mass =
     3
         0
     0
           2
 Divide mass by 386?
 1=yes 2=no
 2
```

```
Enter the stiffness matrix name: kk

stiffness =

500000 -100000

-100000 400000

Natural Frequencies (Hz)

59.39

75.9

Modes Shapes (column format)

QE =

-0.4792 -0.3220

-0.3943 0.5869
```





The curve is the steady-state displacement at coordinate I due to a harmonic force excitation only at coordinate I.



Figure B-3.



Figure B-4.

The curve is the steady-state displacement at coordinate *1* due to a harmonic force excitation only at coordinate *2*.

Due to reciprocity, it is also the steady-state displacement at coordinate 2 due to a harmonic force excitation only at coordinate 1.



Figure B-5.





The curve is the steady-state displacement at coordinate 2 due to a harmonic force excitation only at coordinate 2.



Figure B-7.